



LABORATORY OF  
APPLIED MATHEMATICAL  
PROGRAMMING AND STATISTICS



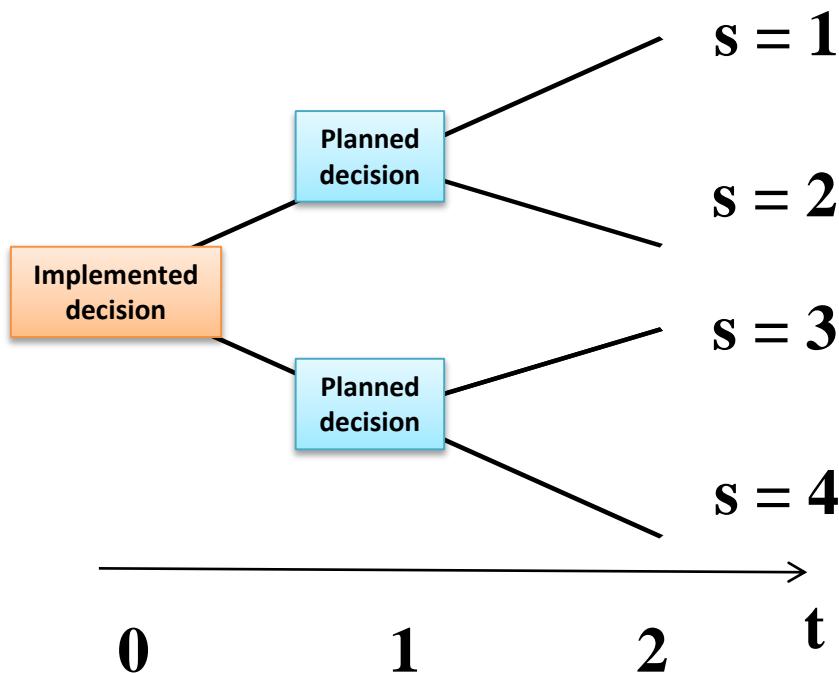
## On the cost and side effects of time inconsistency in long-term hydrothermal planning

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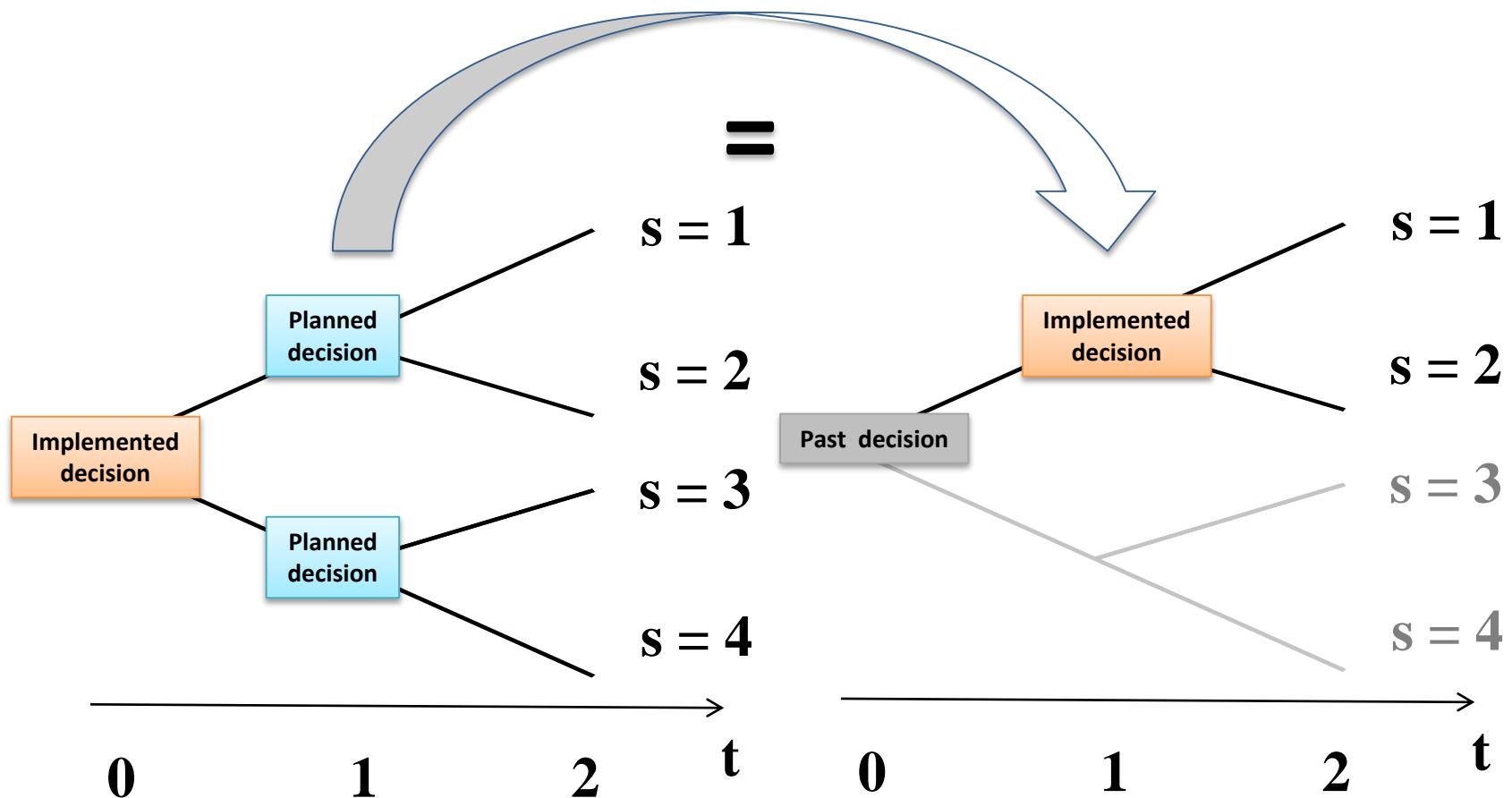
# Time consistent policy

*"a policy is time consistent if and only if future planned decisions are actually going to be implemented"*

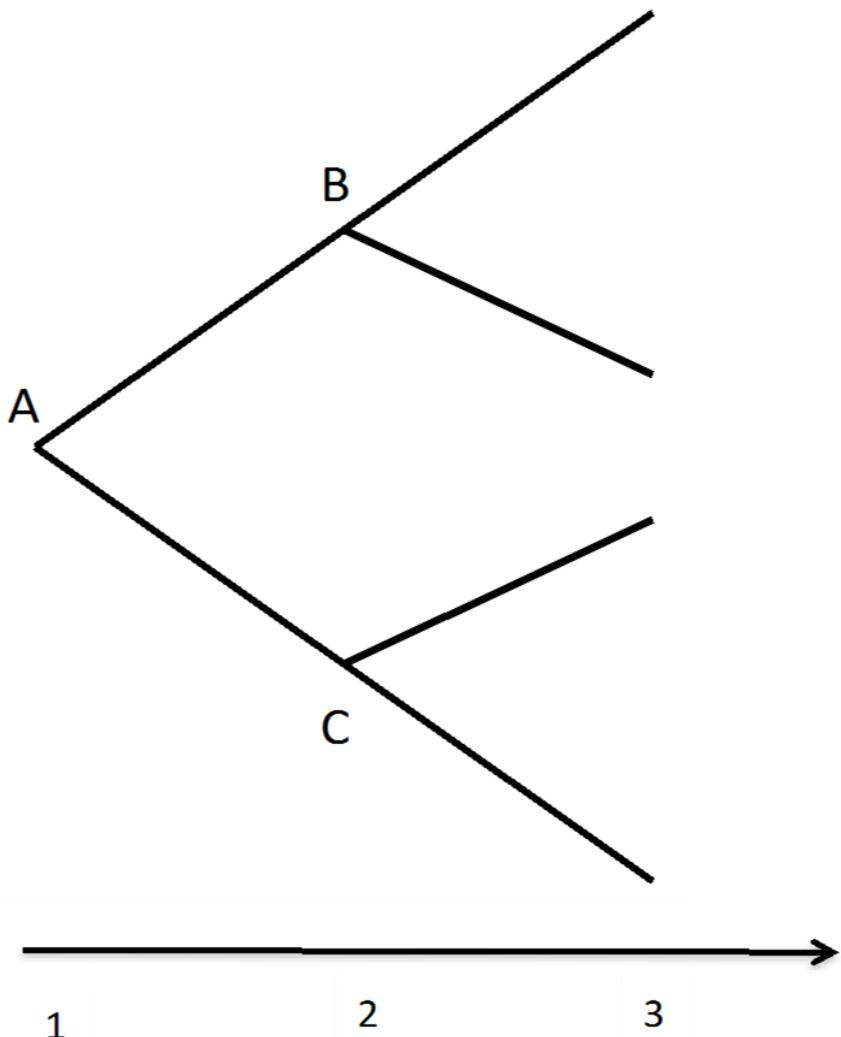


# Time consistent policy

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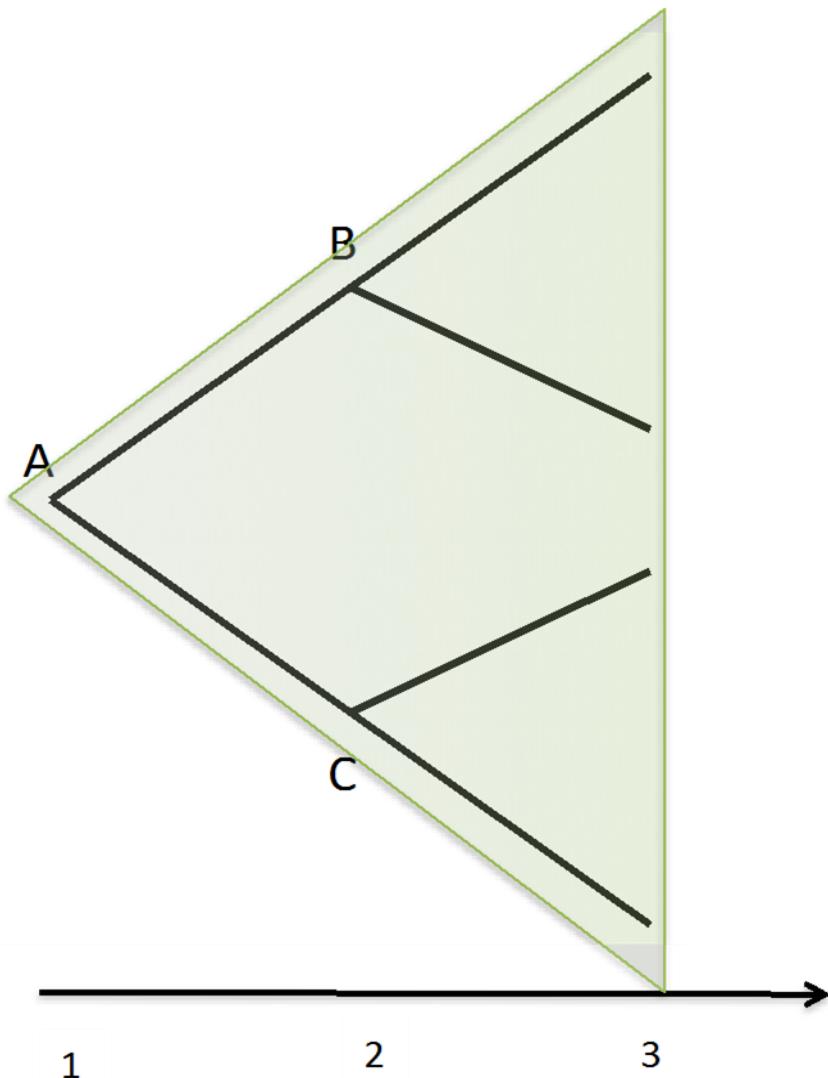


# Dynamic stochastic programming context



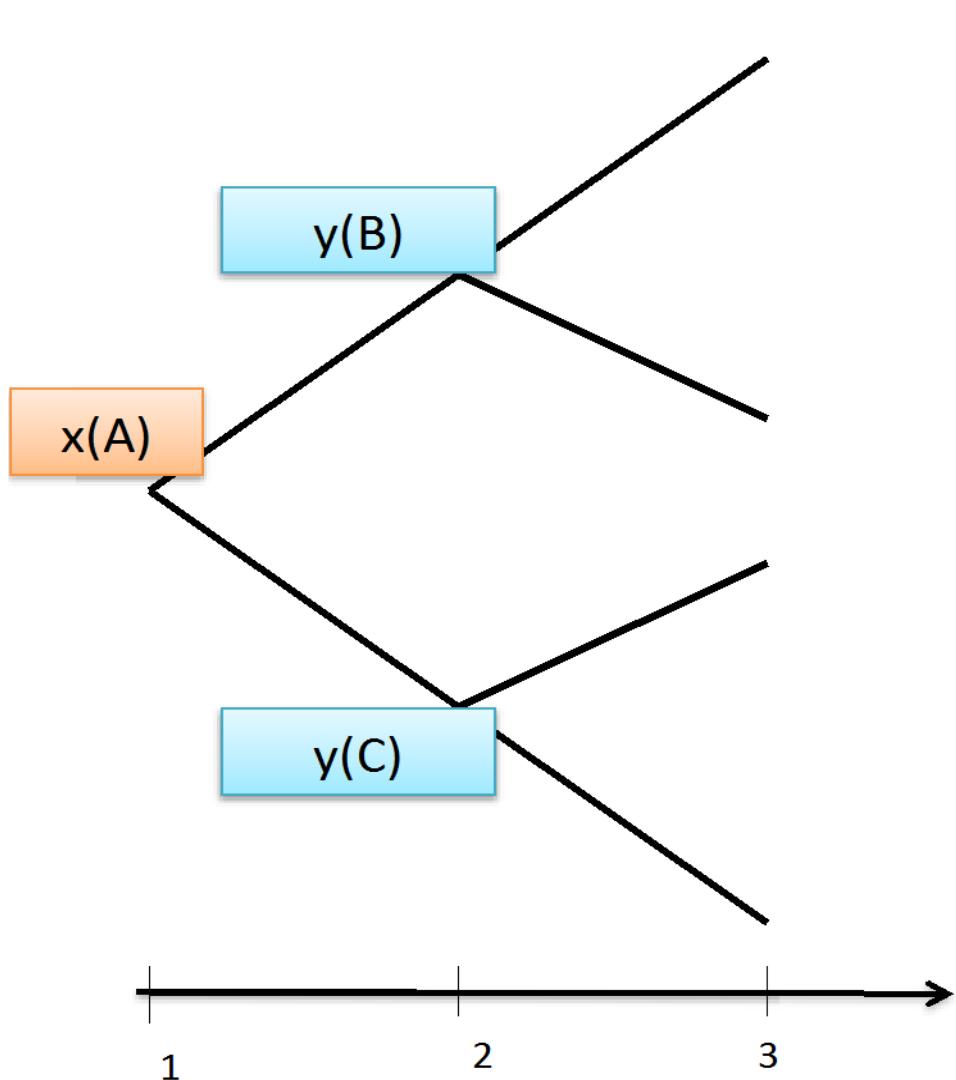
- For each node (A,B,C), decision maker:
  - Defines a multistage problem to be solved
    - $P_1$ ,  $P_2(B)$  and  $P_2(C)$
  - Obtain
    - Implemented decision
    - Planned policy

# Dynamic stochastic programming context



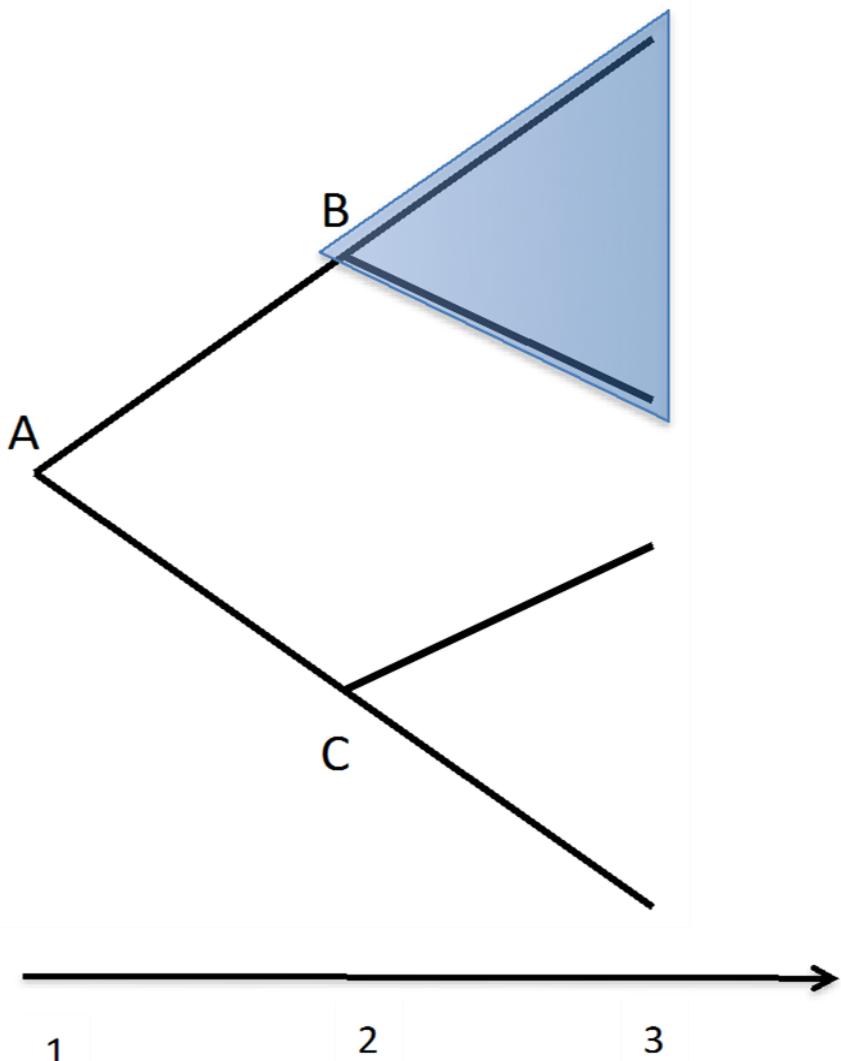
- For problem  $P_1$ ,  
decision maker obtain:

# Dynamic stochastic programming context



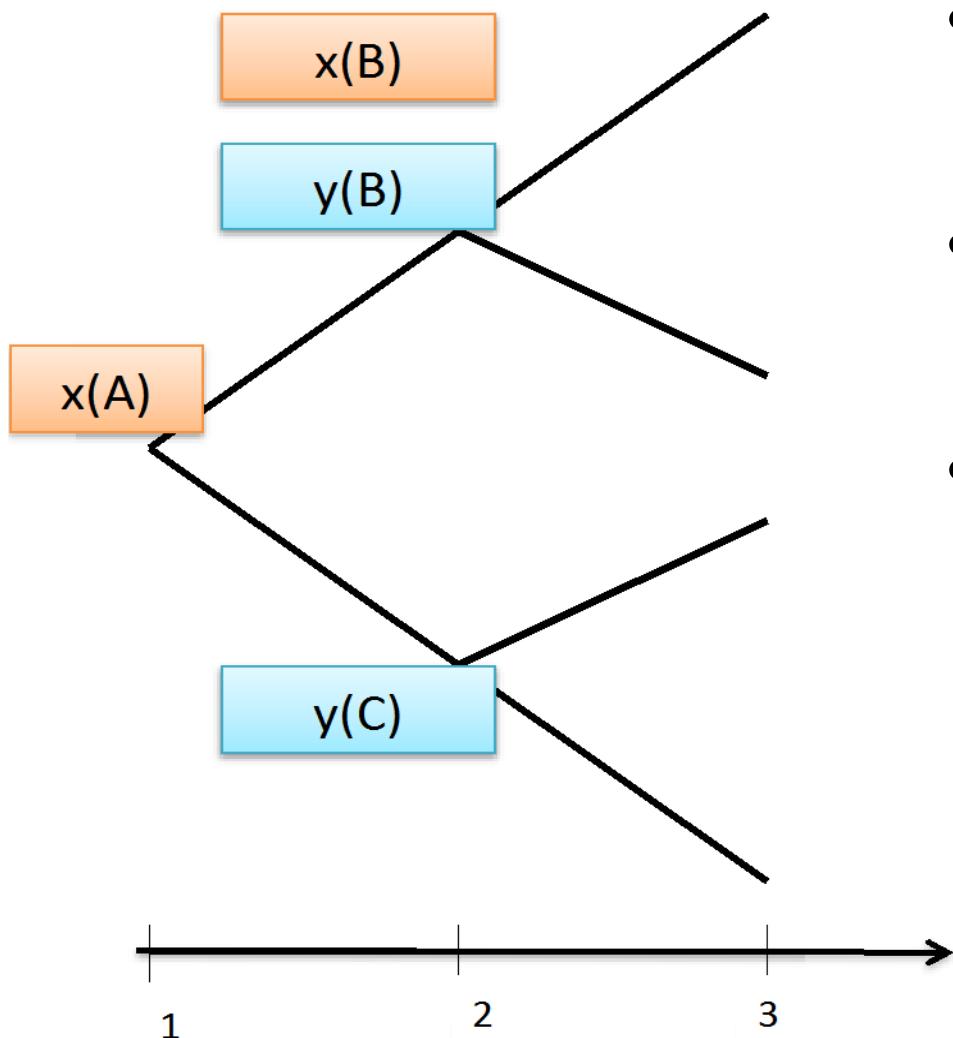
- For problem  $P_1$ ,  
decision maker obtain:
  - Optimal solution of all  
nodes (A,B and C)
  - Implemented decision
    - $x(A)$
  - Planned decisions
    - $y(B)$  and  $y(C)$

# Dynamic stochastic programming context



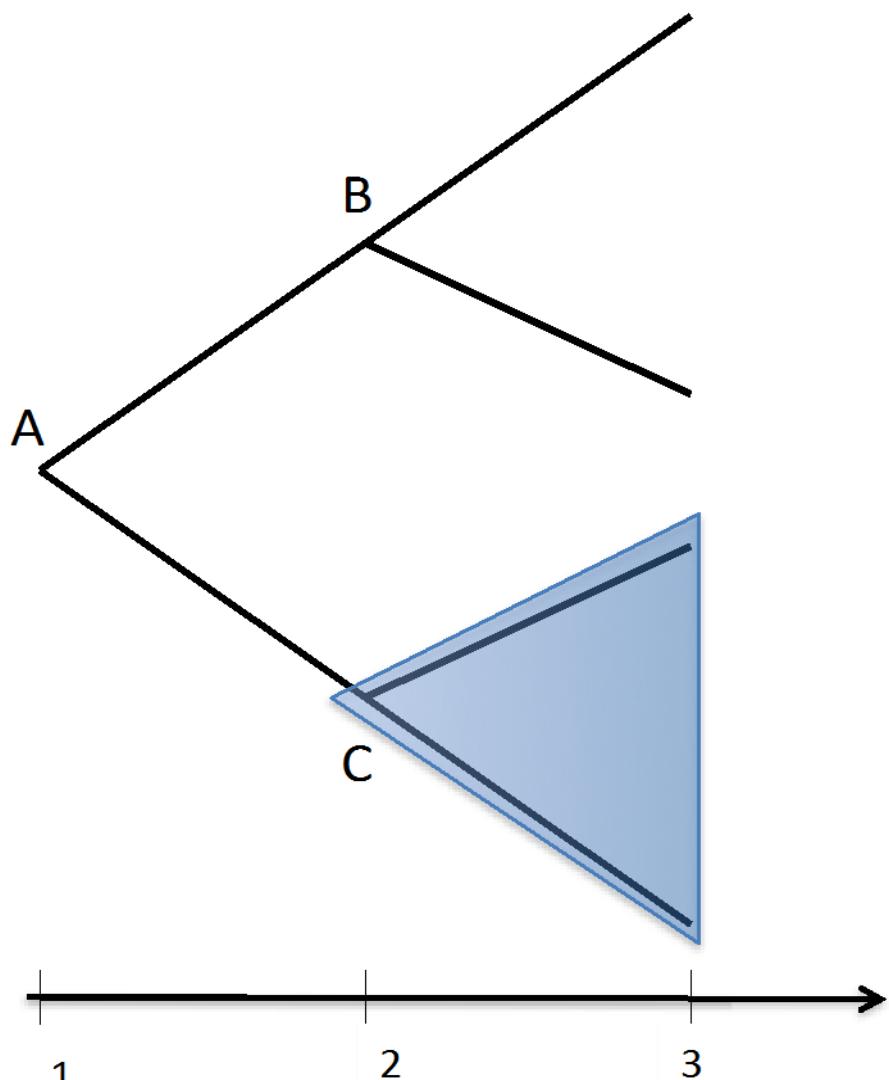
- Given the implemented decision  $x(A)$ .
- Given uncertainty realization B
- Decision maker solves  $P_2(B)$  and obtains:

# Dynamic stochastic programming context



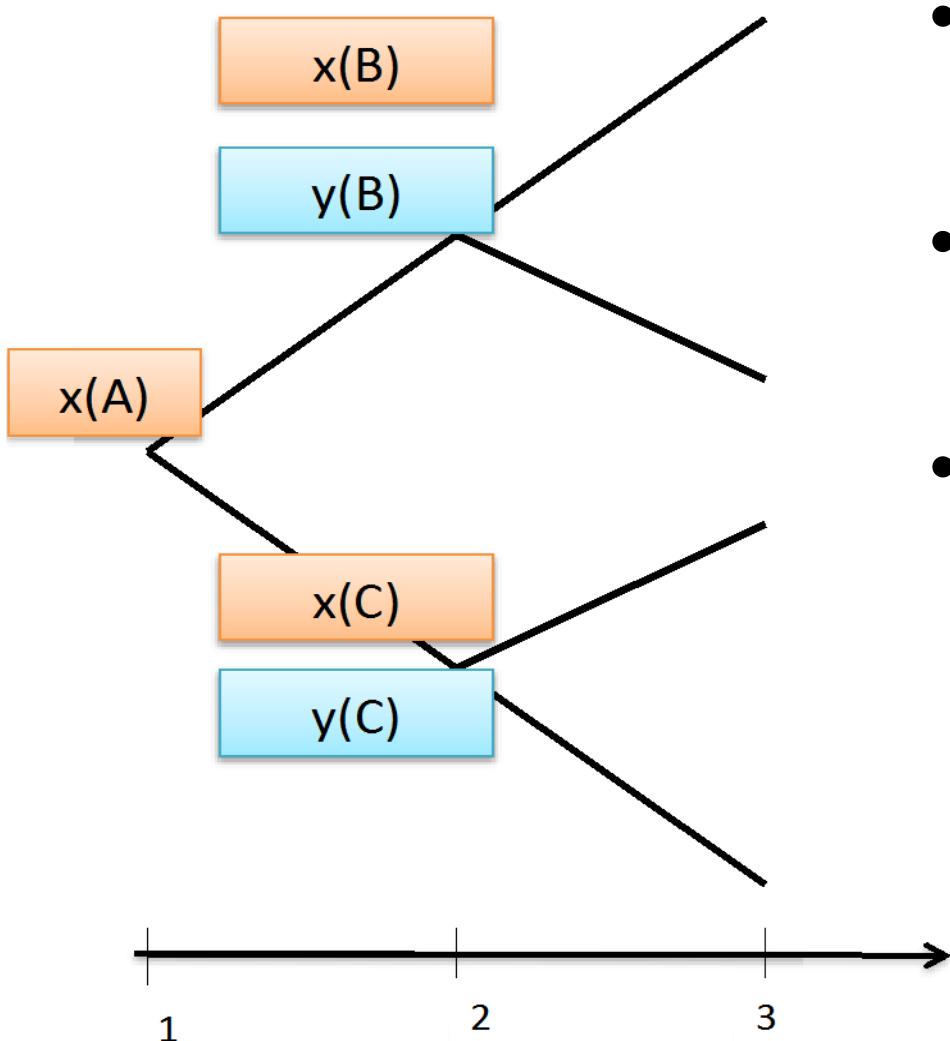
- Given the implemented decision  $x(A)$ :
- Given uncertainty realization  $B$
- Decision maker solves  $P_2(B)$  and obtains:
  - The implemented decision
    - $x(B)$

# Dynamic stochastic programming context



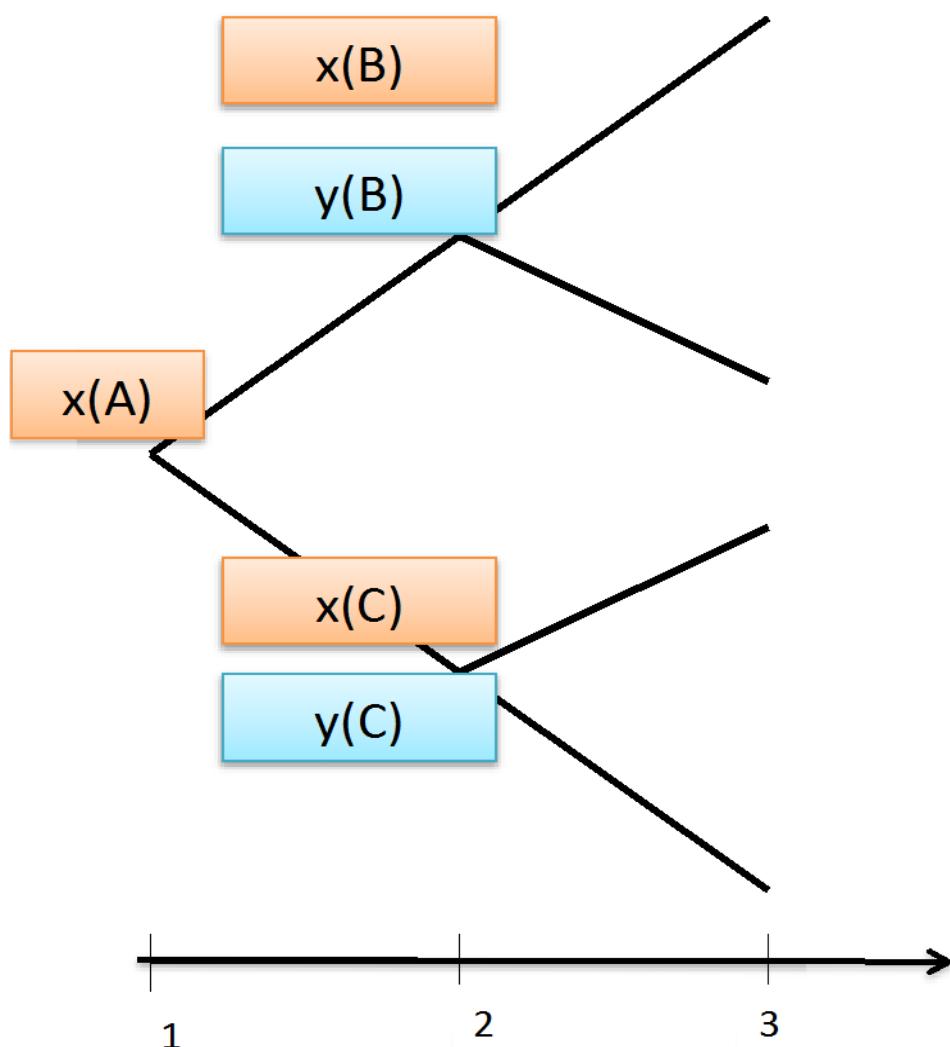
- Given the implemented decision  $x(A)$ .
- Given uncertainty realization  $C$
- Decision maker solves  $P_2(C)$  and obtains:

# Dynamic stochastic programming context



- Given the implemented decision  $x(A)$ .
- Given uncertainty realization C
- Decision maker solves  $P_2(C)$  and obtains:
  - The implemented decision
    - $x(C)$

# Dynamic stochastic programming context



- Time consistency requires

$$x(B) = y(B)$$

$$x(C) = y(C)$$

# Objectives

To characterize modeling simplifications in the planning step, in contrast to the model used in the implementation step, as a possible source of time inconsistency

# Stochastic Dual Dynamic Programming

- Uncertainties:

- Inflows:  $\Omega_t = \{1, 2, \dots, N_t\}$  each with probability  $p_{t,\omega}$ .

- Sampling one scenario  $\omega_t \in \Omega_t$ :

$$Q_t(v_{t-1}, w_{t,\omega}) = \min_{g_t, y_t, f_t} c_t g_t + Q_{t+1}(v_t)$$

Subject to:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1} + w_{t,\omega}: (\pi_{t,\omega})$$

$$(y_t, g_t, f_t) \in \mathcal{X}_t .$$

$$\rightarrow y_t = \begin{bmatrix} v_t \\ u_t \\ s_t \end{bmatrix}$$

- $Q_{t+1}(v_t) = \sum_{\omega \in \Omega_{t+1}} p_{t+1,\omega} Q_{t+1}(v_t, w_{t+1,\omega}).$

# Forward step

$$\min_{g_t, y_t, f_t, \alpha_{t+1}} c_t g_t + \alpha_{t+1}$$

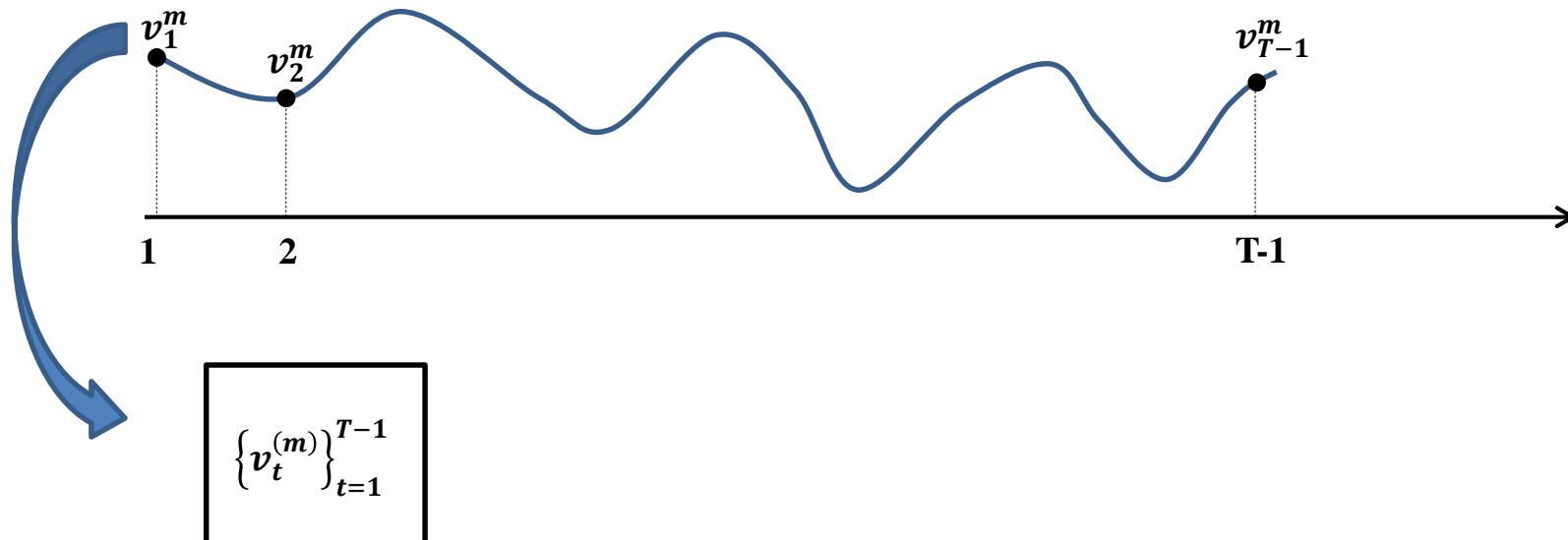
Subject to

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1}^{(m)} + w_{t,\omega}$$

$$\alpha_{t+1} \geq \tilde{Q}_{t+1}^{(k)} \left( v_t^{(k)} \right) + \left( \tilde{\pi}_{t+1}^{(k)} \right)^T \left( v_t - v_t^{(k)} \right); \forall k \in \mathcal{K}^{(m)}$$

$$(y_t, g_t, f_t) \in \mathcal{X}_t .$$



# Backward Step

$$\tilde{Q}_t^{(m)}(v_{(t-1)}, w_{t,\omega}) = \min_{g_t, y_t, f_t, \alpha_{t+1}} c_t g_t + \alpha_{t+1}$$

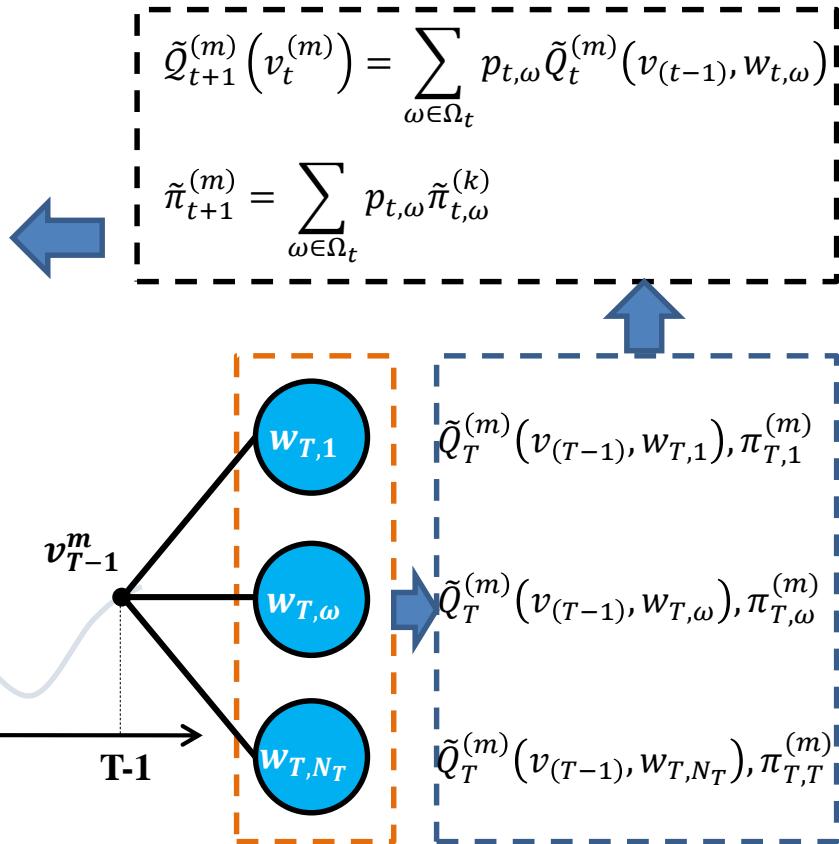
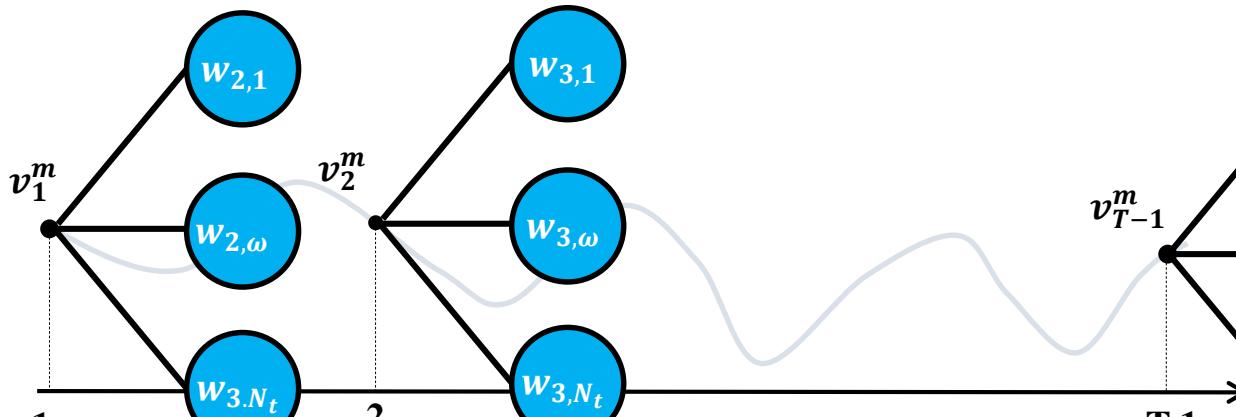
Subject to:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

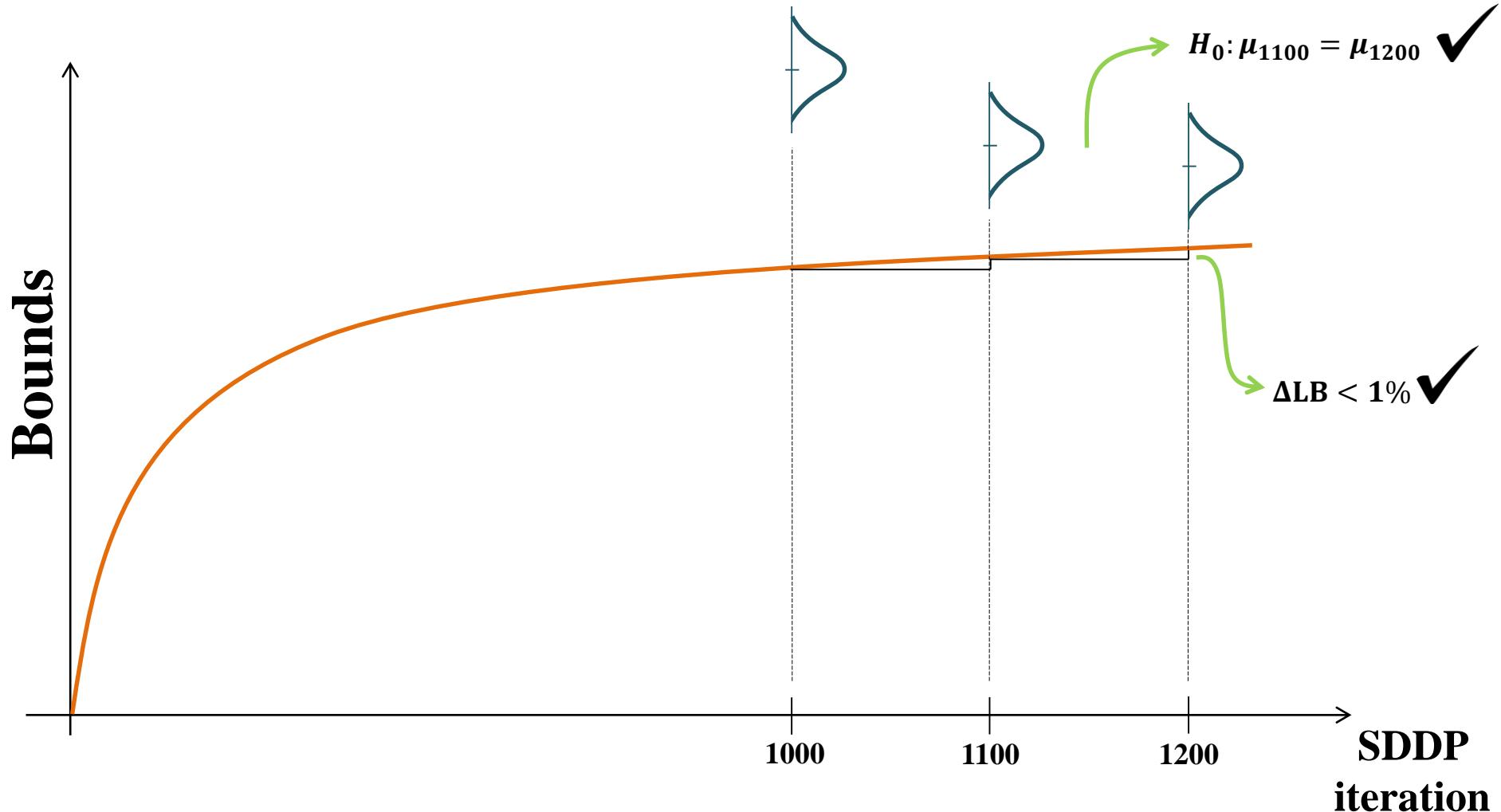
$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1}^{(m)} + w_{t,\omega} : (\tilde{\pi}_{t,\omega}^{(k)})$$

$$\alpha_{t+1} \geq \tilde{Q}_{t+1}^{(k)}(v_t^{(k)}) + (\tilde{\pi}_{t+1}^{(k)})^\top (v_t - v_t^{(k)}) ; \forall k \in \mathcal{K}^{(m)}$$

$$(y_t, g_t, f_t) \in \mathcal{X}_t .$$



# Stopping Criterion



## Implementation Model

$$\min_{g_t, y_t, f_t} c_t g_t + \mathcal{Q}_{t+1}^{\text{plan}}(v_t)$$

Subject to

$$\begin{aligned} A_t g_t + B_t y_t + C_t f_t &= d_t \\ v_t + u_t + s_t + M(u_t + s_t) \\ &= v_{t-1} + w_{t,\omega}; (\pi_{t,\omega}) \\ (y_t, g_t, f_t) &\in \mathcal{X}_t^{\text{imp}}. \end{aligned}$$

## Planning Model

$$\min_{g_t, y_t, f_t} c_t g_t + \mathcal{Q}_{t+1}^{\text{plan}}(v_t)$$

Subject to

$$\begin{aligned} A_t g_t + B_t y_t + C_t f_t &= d_t \\ v_t + u_t + s_t + M(u_t + s_t) \\ &= v_{t-1} + w_{t,\omega}; (\pi_{t,\omega}) \\ (y_t, g_t, f_t) &\in \mathcal{X}_t^{\text{plan}}. \end{aligned}$$

# Planning Step in $t$

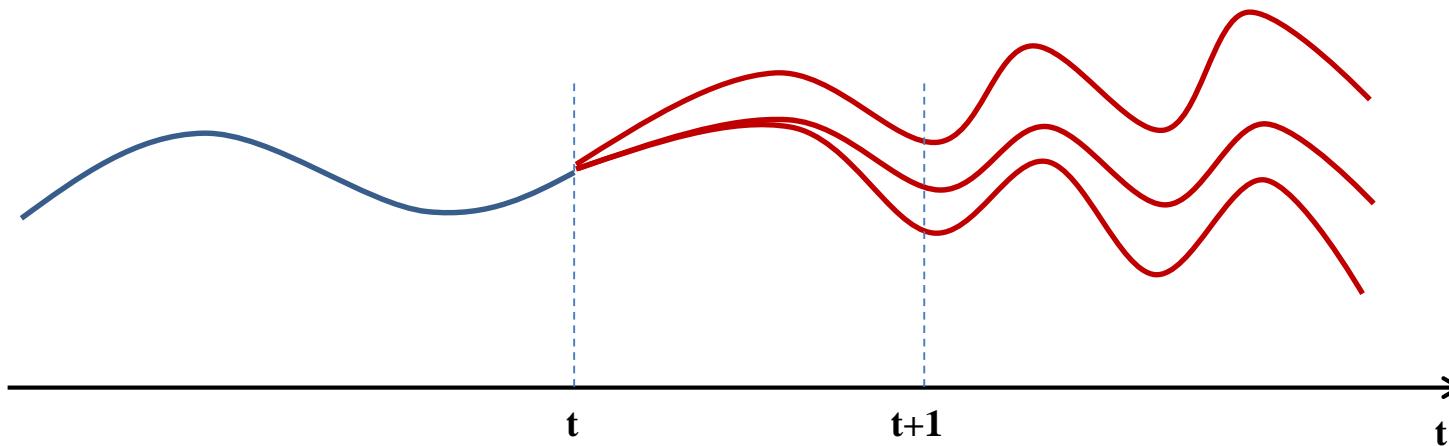
- Solve SDDP using a planning model (simplified)

$$\min_{g_t, y_t, f_t} c_t g_t + Q_{t+1}^S(v_t)$$

Subject to:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

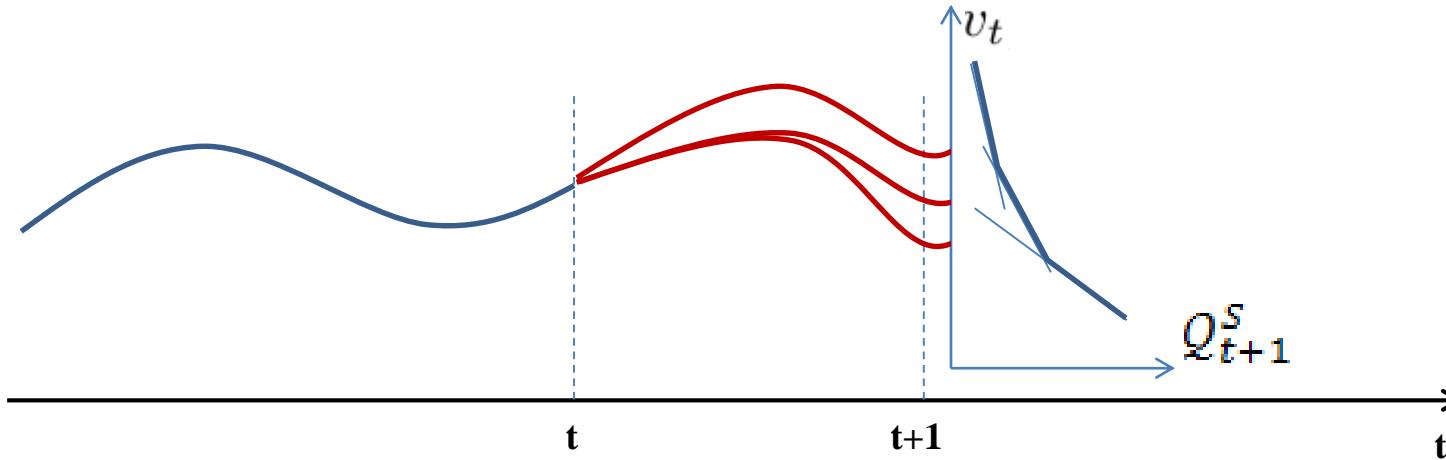
$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1} + w_{t,\omega}; (\pi_{t,\omega}) \\ (y_t, g_t, f_t) \in \mathcal{X}_t^S.$$



# Planning Step in $t$

- Obtain the recourse function for  $t + 1$

$$\begin{aligned} & \min_{g_t, y_t, f_t} c_t g_t + Q_{t+1}^S(v_t) \\ & \text{Subject to} \\ & A_t g_t + B_t y_t + C_t f_t = d_t \\ & v_t + u_t + s_t + M(u_t + s_t) = v_{t-1} + w_{t,\omega}; (\pi_{t,\omega}) \\ & (y_t, g_t, f_t) \in \mathcal{X}_t^S. \end{aligned}$$



## Implementation step in $t$

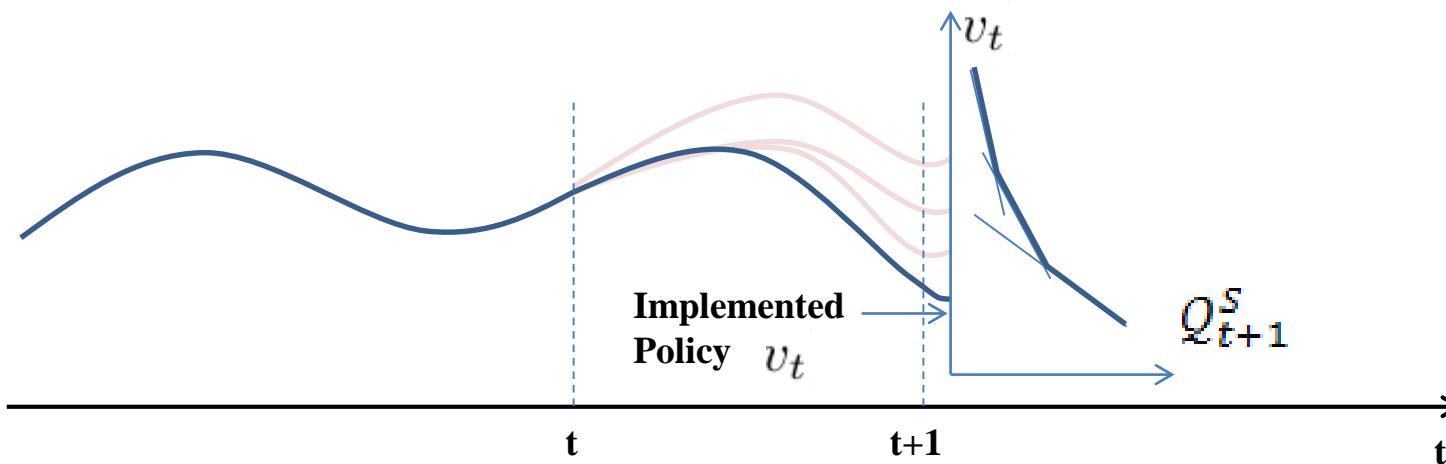
- Uses the recourse function (simplified) for  $t + 1$  and implements the first stage decision using a detailed model.

$$\min_{g_t, y_t, f_t} c_t g_t + Q_{t+1}^S(v_t)$$

Subject to:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1} + w_{t,\omega}; (\pi_{t,\omega})$$
$$(y_t, g_t, f_t) \in \mathcal{X}_t^D.$$



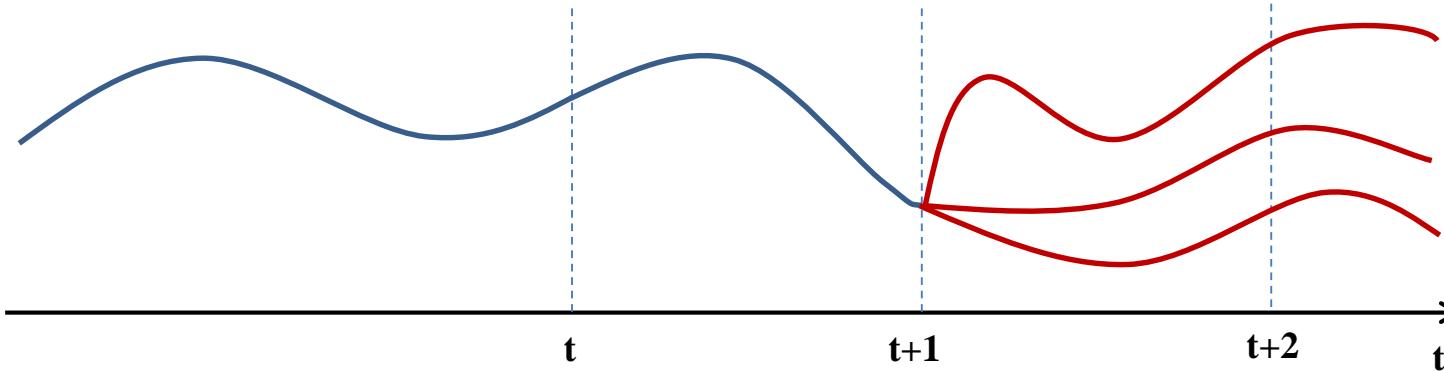
# Planning Step in $t + 1$

- Solve SDDP using a planning model (simplified)

$$\min_{g_{t+1}, y_{t+1}, f_{t+1}} c_{t+1} g_t + Q_{t+2}^S(v_{t+1})$$

Subject to:

$$\begin{aligned} A_{t+1} g_{t+1} + B_{t+1} y_{t+1} + C_{t+1} f_{t+1} &= d_{t+1} \\ v_t + u_t + s_t + M(u_t + s_t) &= v_t + w_{t+1, \omega}; (\pi_{t+1, \omega}) \\ (y_{t+1}, g_{t+1}, f_{t+1}) &\in \mathcal{X}_{t+1}^S. \end{aligned}$$



# Planning Step in $t + 1$

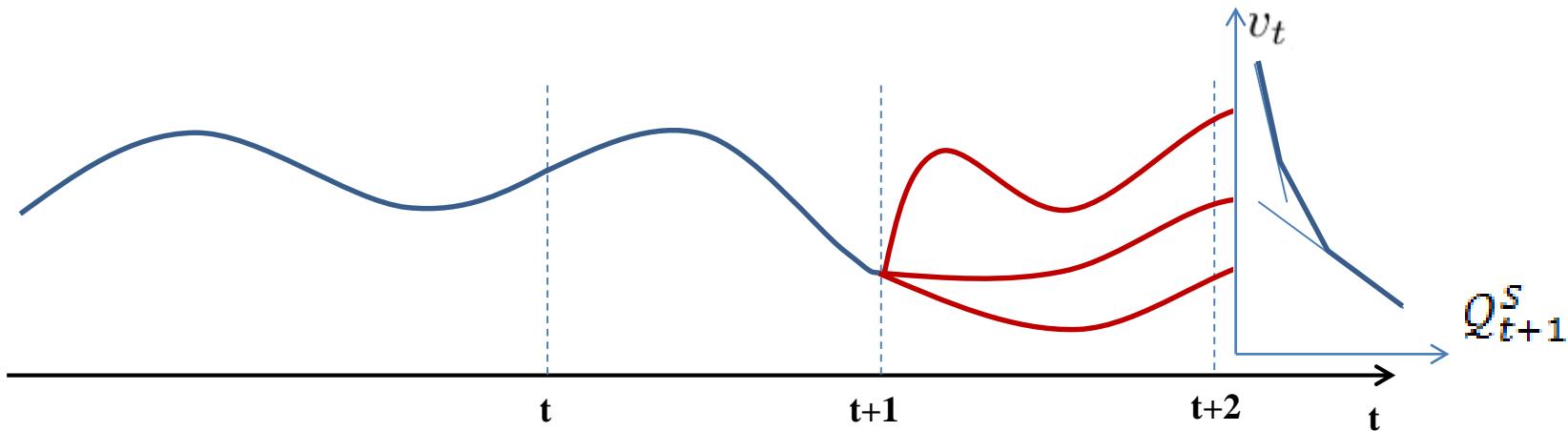
- Obtain the recourse function for  $t + 2$

$$\min_{g_{t+1}, y_{t+1}, f_{t+1}} c_{t+1} g_t + Q_{t+2}^S(v_{t+1})$$

Subject to:

$$A_{t+1}g_{t+1} + B_{t+1}y_{t+1} + C_{t+1}f_{t+1} = d_{t+1}$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_t + w_{t+1,\omega}; (\pi_{t+1,\omega}) \\ (y_{t+1}, g_{t+1}, f_{t+1}) \in \mathcal{X}_{t+1}^S.$$



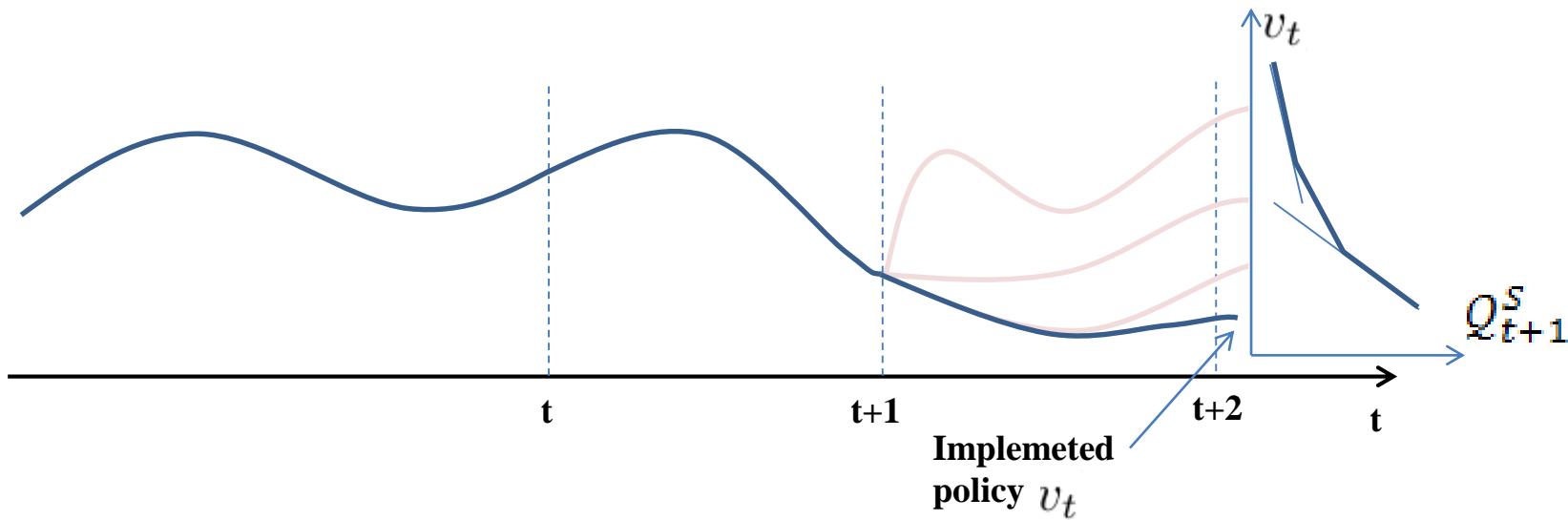
## Implementation step in $t + 1$

- ❑ Uses the recourse function (simplified) for  $t + 2$  and implements the first stage decision using a detailed model.

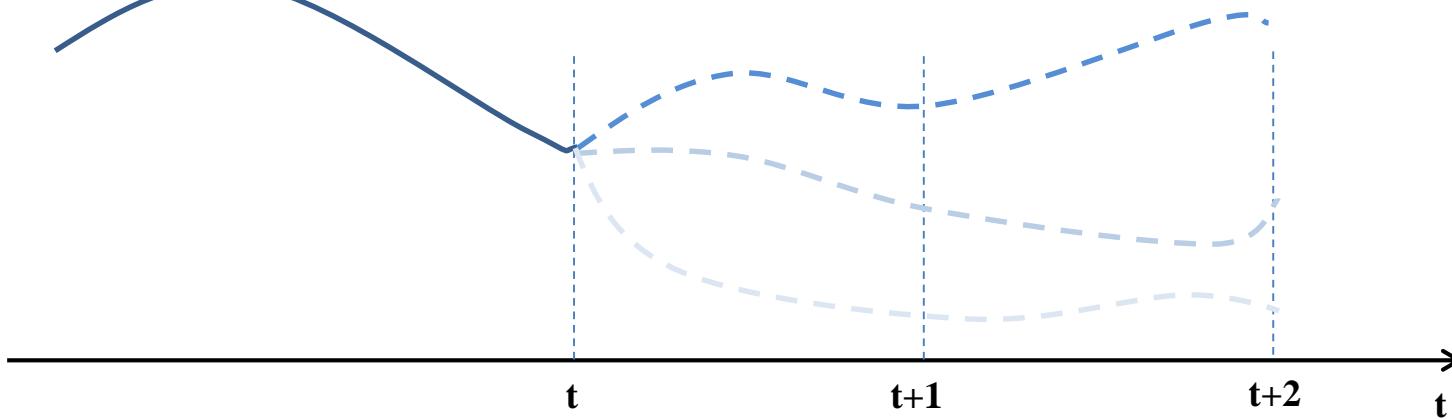
$$\min_{g_{t+1}, y_{t+1}, f_{t+1}} c_{t+1} g_t + Q_{t+2}^S(v_{t+1})$$

Subject to:

$$\begin{aligned} A_{t+1} g_{t+1} + B_{t+1} y_{t+1} + C_{t+1} f_{t+1} &= d_{t+1} \\ v_t + u_t + s_t + M(u_t + s_t) &= v_t + w_{t+1,\omega}; (\pi_{t+1,\omega}) \\ (y_{t+1}, g_{t+1}, f_{t+1}) &\in \mathcal{X}_{t+1}^D \end{aligned}$$



## Uncertainty in inflow realization in the implementation step



$$\xrightarrow{\text{blue arrow}} \mathcal{P}(\{\mathcal{Q}_{t+1}^{plan}\}_{t=1}^T, \{\mathcal{X}_t^{imp}\}_{t=1}^T, \{w_{t,\omega}\}_{t,\omega=1}^{T,M}).$$

# Simulating the implemented policy

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SDDP method extended to a rolling-horizon scheme

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- 1: Sample  $M$  inflow paths,  $\{\mathbf{w}_{t,\omega}\}_{t,\omega=1}^{T,M}$ .
  - 2: Set  $t = 1$  and initial conditions to  $\{v_{0,\omega}\}_{\omega=1}^M$ .
  - 3: **for** each sampled path  $\omega = 1, \dots, M$  **do**
  - 4:     Converge SDDP with  $\mathcal{X}_\tau \leftarrow \mathcal{X}_\tau^{plan} \forall \tau \geq t$ .
  - 5:     Store the recourse function  $\mathcal{Q}_{t+1}^{plan}$ .
  - 6:     Solve the implementation problem for period  $t$  using  $\mathcal{Q}_{t+1}^{plan}$ .
  - 7:     Update  $\mathcal{P}(\{\mathcal{Q}_t^{plan}\}_{t=1}^T, \{\mathcal{X}_t^{imp}\}_{t=1}^T, \{\mathbf{w}_{t,\omega}\}_{t,\omega=1}^{T,M})$ .
  - 8: **end for**
  - 9:  $t \leftarrow t + 1$ .
  - 10: **if**  $t = T + 1$  **then**
  - 11:     STOP.
  - 12: **else**
  - 13:     Set initial conditions to  $\{v_{t-1,\omega}^*\}_{\omega=1}^M$  stored in  $\mathcal{P}$ .
  - 14:     Go to step 3.
  - 15: **end if**
-

# Fast algorithm – Forward Step

$$\min_{g_t, y_t, f_t, \alpha_{t+1}} c_t g_t + \alpha_{t+1}$$

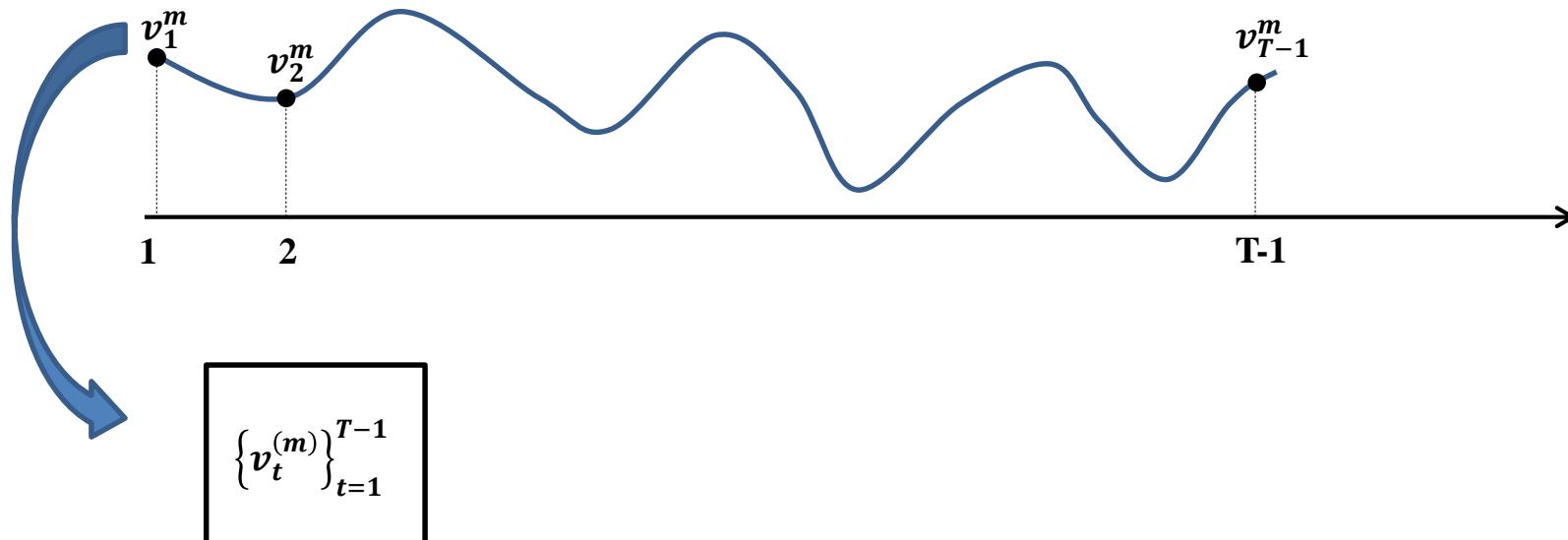
Subject to:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1}^{(m)} + w_{t,\omega}$$

$$\alpha_{t+1} \geq \tilde{\mathcal{Q}}_{t+1}^{(k)} \left( v_t^{(k)} \right) + \left( \tilde{\pi}_{t+1}^{(k)} \right)^T \left( v_t - v_t^{(k)} \right); \forall k \in \mathcal{K}^{(m)}$$

$$(y_t, g_t, f_t) \in \mathcal{X}^D_t .$$



# Fast Algorithm – Backward Step

$$\tilde{Q}_t^{(m)}(v_{(t-1)}, w_{t,\omega}) = \min_{g_t, y_t, f_t, \alpha_{t+1}} c_t g_t + \alpha_{t+1}$$

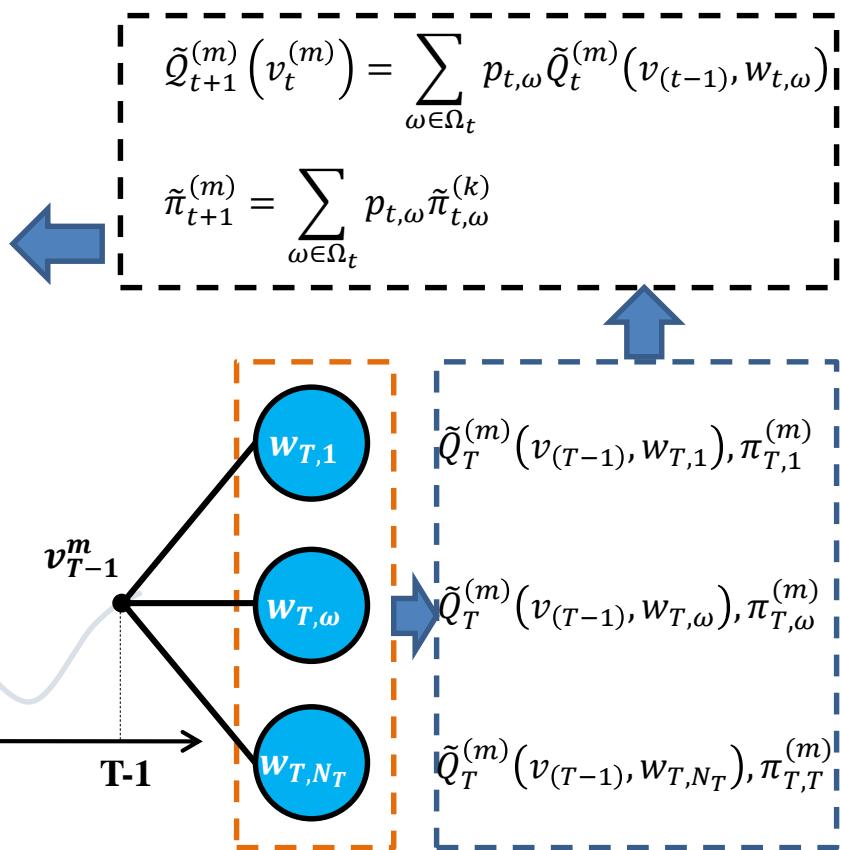
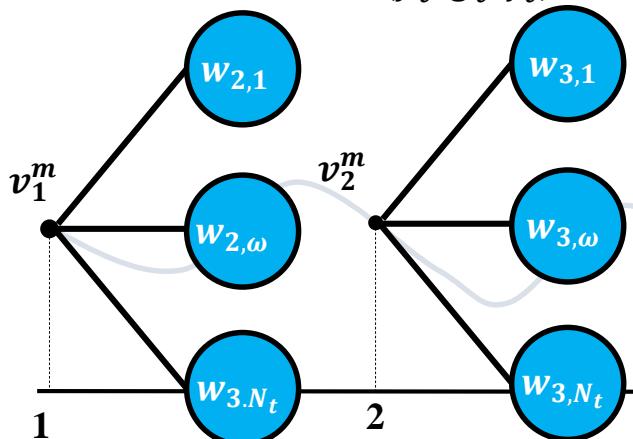
sujeto a:

$$A_t g_t + B_t y_t + C_t f_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1}^{(m)} + w_{t,\omega} : (\tilde{\pi}_{t,\omega}^{(k)})$$

$$\alpha_{t+1} \geq \tilde{Q}_{t+1}^{(k)}(v_t^{(k)}) + (\tilde{\pi}_{t+1}^{(k)})^\top (v_t - v_t^{(k)}) ; \forall k \in \mathcal{K}^{(m)}$$

$$(y_t, g_t, f_t) \in \mathcal{X}^S_t .$$



# Time Inconsistency Gap

- The inconsistency gap is:

$$GAP = \frac{1}{M} \sum_{t=1}^T \sum_{\omega=1}^M c_t^\top g_{t,\omega}^D - \frac{1}{M} \sum_{t=1}^T \sum_{\omega=1}^M c_t^\top g_{t,\omega}^S$$

- There exists the possibility that the gap is due to a sampling error:

$$\begin{cases} H_0: \mu^D = \mu^S \\ H_1: \mu^D \neq \mu^S \end{cases}$$

- The null hypothesis is accepted if  $0 \in [GAP \pm 1.96 \cdot \sqrt{(\frac{S_D^2 + S_S^2}{M})}]$

# Simplification Example – Kircchoff's Voltage Law

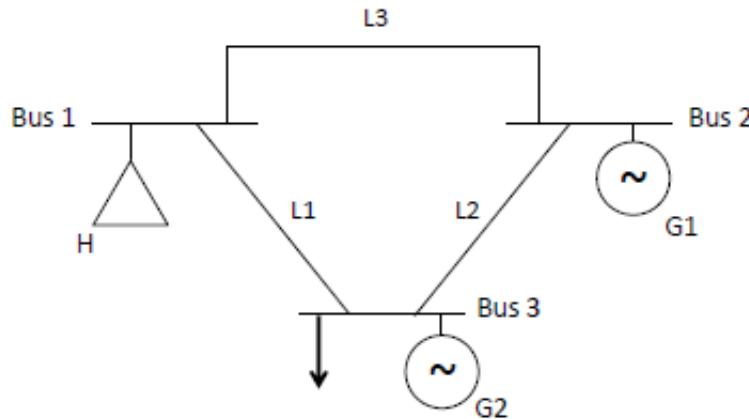
- Simplified model  $\mathcal{X}_t^S$  :

$$\begin{aligned}\mathcal{X}_t^S = \{ & (y_t, g_t, f_t) | \\ & \underline{V} \leq v_t \leq \bar{V} \\ & \underline{U} \leq u_t \leq \bar{U} \\ & \underline{S} \leq s_t \leq \bar{S} \\ & \underline{G} \leq g_t \leq \bar{G} \\ & -\bar{F} \leq f_t \leq \bar{F}\}.\end{aligned}$$

- Detailed model  $\mathcal{X}_t^D$  :

$$\mathcal{X}_t^D = \mathcal{X}_t^S \cap \{(y_t, g_t, f_t, \theta_t) | f_t = S\theta_t\}.$$

# System



- $T = 60$ . (Last 12 periods are discarded).
- $D = 100\text{MWh}$ .

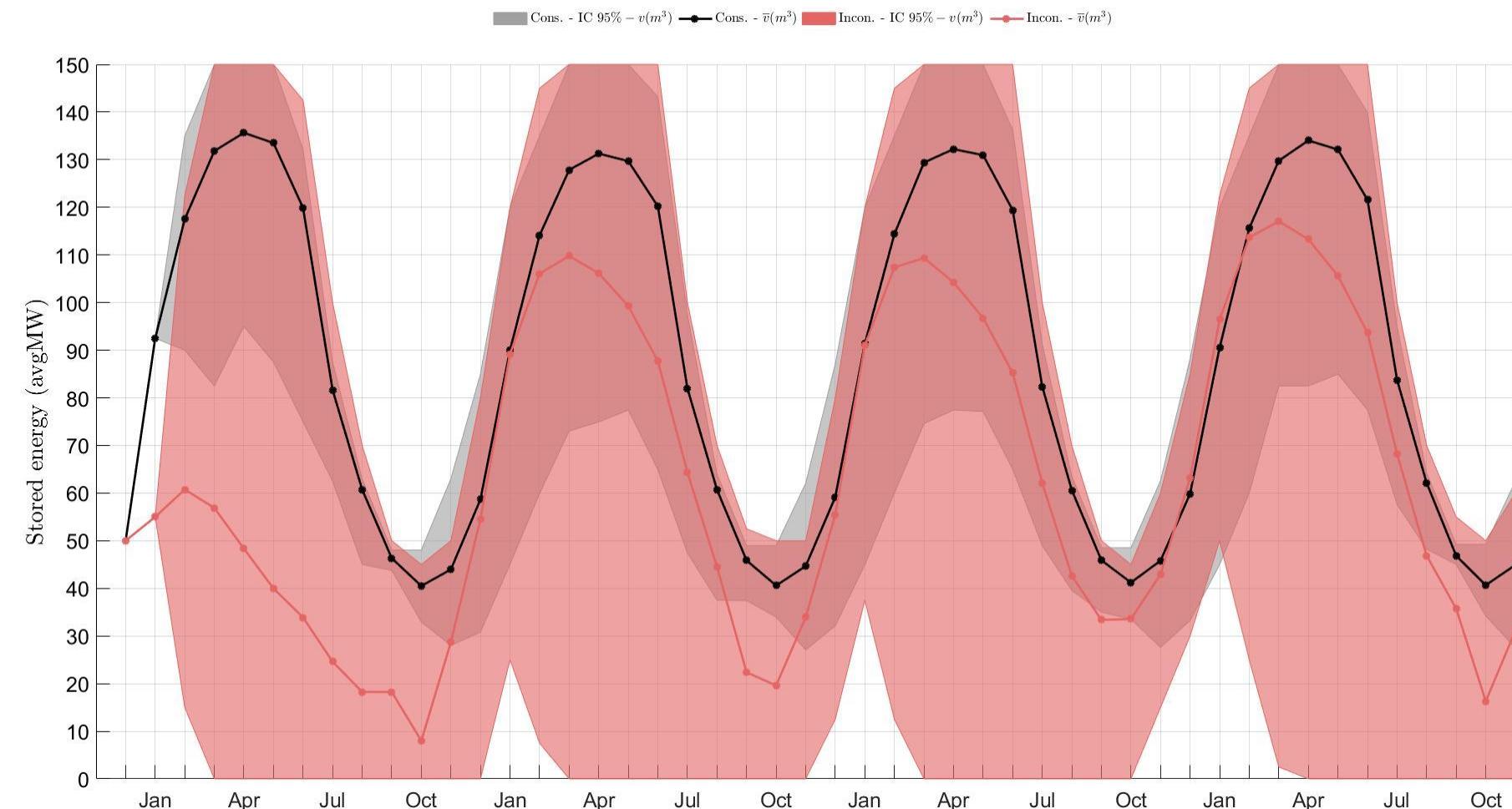
Thermal Generator	$c$ R\$/MWh	$\bar{G}$ MW
$G_1$	20	100
$G_2$	100	55
Hydro Generator	$\bar{V}$ $m^3$	$\bar{U}$ $m^3$
$H$	150	80

TL	From	To	$\bar{F}$ MW	Reactance (pu)
1	1	3	100	1
2	2	3	65	0.5
3	1	2	25	1

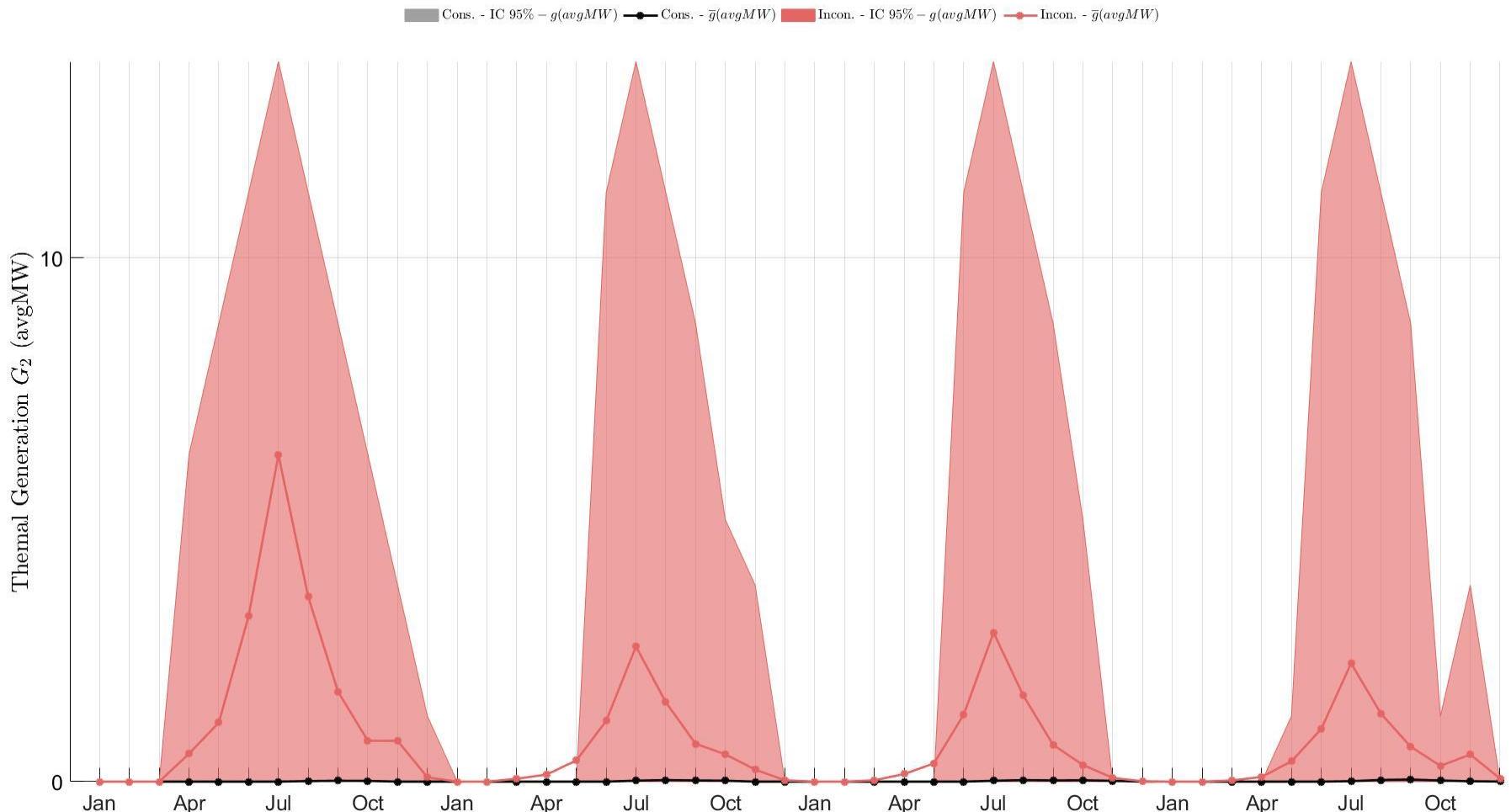
# GAP

**GAP: MMR\$174.4**  
**GAP confidence interval: MMR\$[174.05 174.55]**

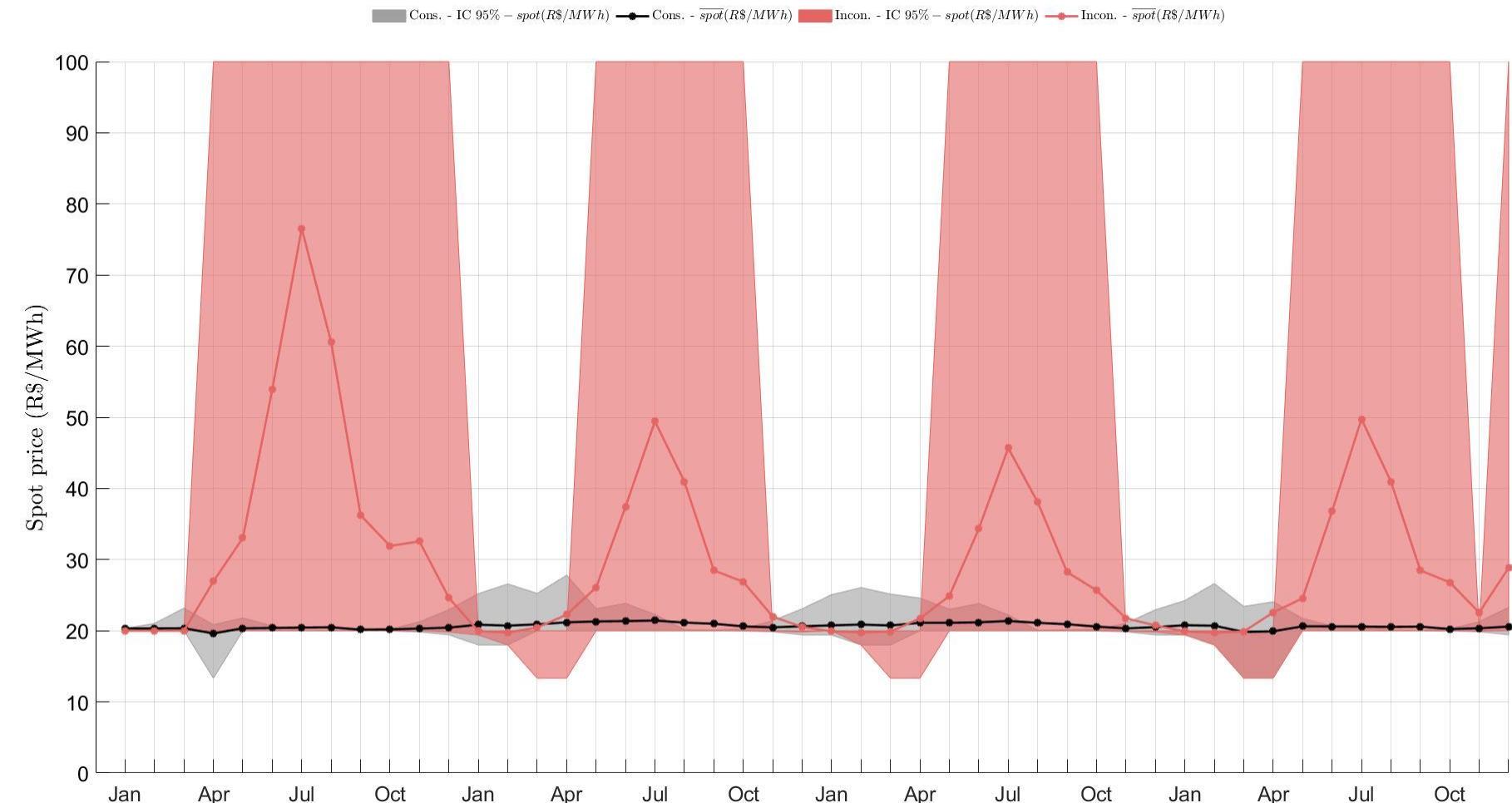
# Stored energy



# Thermal Generation $G_2$



# Spot price



# Simplification Example – Security Criteria

$$\min c_t^T g_t + C^{Imb} \delta + \alpha_{t+1}$$

Subject to:

## Pre-Contingency

$$\begin{aligned} Ag_t + By_t + Cf_t &= d_t \\ v_t + u_t + s_t + M(u_t + s_t) &= v_{t-1} + w_{t,\omega}: (\tilde{\pi}_{t,\omega}^{(m)}) \\ f_t &= S\theta_t \\ -F \leq f_t \leq F \\ g_t \leq \bar{G}, u_t \leq \bar{U}, v_t \leq \bar{V} \end{aligned}$$

## Post-Contingency

$$\begin{aligned} A^c g_t^c + B^c u_t^c + C^c f_t^c + \phi_t^{c+} - \phi_t^{c-} &= d_t; \forall c \in \mathcal{C} \\ v_t^c + u_t^c + s_t^c + M(u_t^c + s_t^c) &= v_{t-1} + w_{t,\omega}: (\tilde{\pi}_{t,\omega}^{c,(m)}); \forall c \in \mathcal{C} \\ f_t^c &= S^c \theta_t^c; \forall c \in \mathcal{C} \\ v_t^c \leq \bar{V}; \forall c \in \mathcal{C} \\ -Z_l^c \bar{F}_l \leq f_t^c \leq Z_l^c \bar{F}_l; \forall c \in \mathcal{C} \\ ||g_t - g_t^c|| &\leq Z_g^c R_g; \forall c \in \mathcal{C} \\ ||u_t - u_t^c|| &\leq Z_u^c R_u; \forall c \in \mathcal{C} \\ \delta &\geq \phi_t^{+c} + \phi_t^{-c}; \forall c \in \mathcal{C} \end{aligned}$$

## Cut

$$\alpha_{t+1} \geq \tilde{\mathcal{Q}}_{t+1}^{(k)} \left( v_t^{(k)} \right) + \left( \tilde{\pi}_{t+1}^{(k)} + \sum_{c \in \mathcal{C}} \tilde{\pi}_{t+1}^{c,(k)} \right)^T \left( v_t - v_t^{(k)} \right); \forall k \in \mathcal{K}^{(m)}$$

# Simplification Example – Security Criteria

$$\min c_t^T g_t + C^{Imb} \delta + \alpha_{t+1}$$

Subject to:

$x_t^{plan}$

$x_t^{imp}$

## Pre-Contingency

$$Ag_t + By_t + Cf_t = d_t$$

$$v_t + u_t + s_t + M(u_t + s_t) = v_{t-1} + w_{t,\omega}: (\tilde{\pi}_{t,\omega}^{(m)})$$

$$f_t = S\theta_t$$

$$\frac{-F}{-F} \leq f_t \leq \frac{F}{F}$$

$$g_t \leq \overline{G}, u_t \leq \overline{U}, v_t \leq \overline{V}$$

## Post-Contingency

$$A^c g_t^c + B^c u_t^c + C^c f_t^c + \phi_t^{c+} - \phi_t^{c-} = d_t; \forall c \in \mathcal{C}$$

$$v_t^c + u_t^c + s_t^c + M(u_t^c + s_t^c) = v_{t-1} + w_{t,\omega}: (\tilde{\pi}_{t,\omega}^{c,(m)}); \forall c \in \mathcal{C}$$

$$f_t^c = S^c \theta_t^c; \forall c \in \mathcal{C}$$

$$v_t^c \leq \overline{V}; \forall c \in \mathcal{C}$$

$$-Z_l^c \overline{F}_l \leq f_t^c \leq Z_l^c \overline{F}_l; \forall c \in \mathcal{C}$$

$$||g_t - g_t^c|| \leq Z_g^c R_g; \forall c \in \mathcal{C}$$

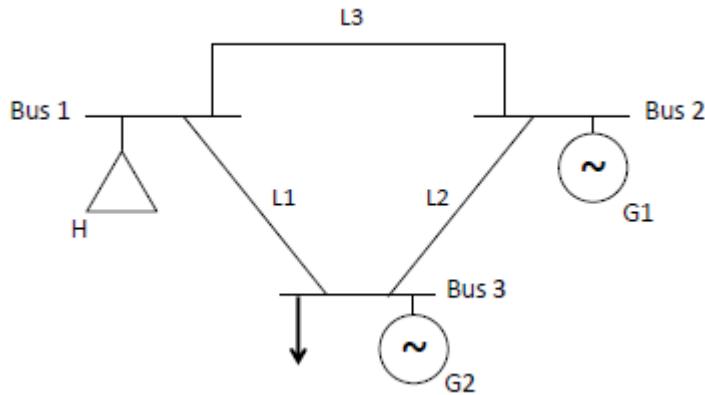
$$||u_t - u_t^c|| \leq Z_u^c R_u; \forall c \in \mathcal{C}$$

$$\delta \geq \phi_t^{+c} + \phi_t^{-c}; \forall c \in \mathcal{C}$$

## Cut

$$\alpha_{t+1} \geq \tilde{\mathcal{Q}}_{t+1}^{(k)} \left( v_t^{(k)} \right) + \left( \tilde{\pi}_{t+1}^{(k)} + \sum_{c \in \mathcal{C}} \tilde{\pi}_{t+1}^{c,(k)} \right)^T \left( v_t - v_t^{(k)} \right); \forall k \in \mathcal{K}^{(m)}$$

# System



- $T = 60$ . (Last 12 periods are discarded).
- $D = 100\text{MWh}$ .
- **Using  $n - 1$  in transmission lines only.**

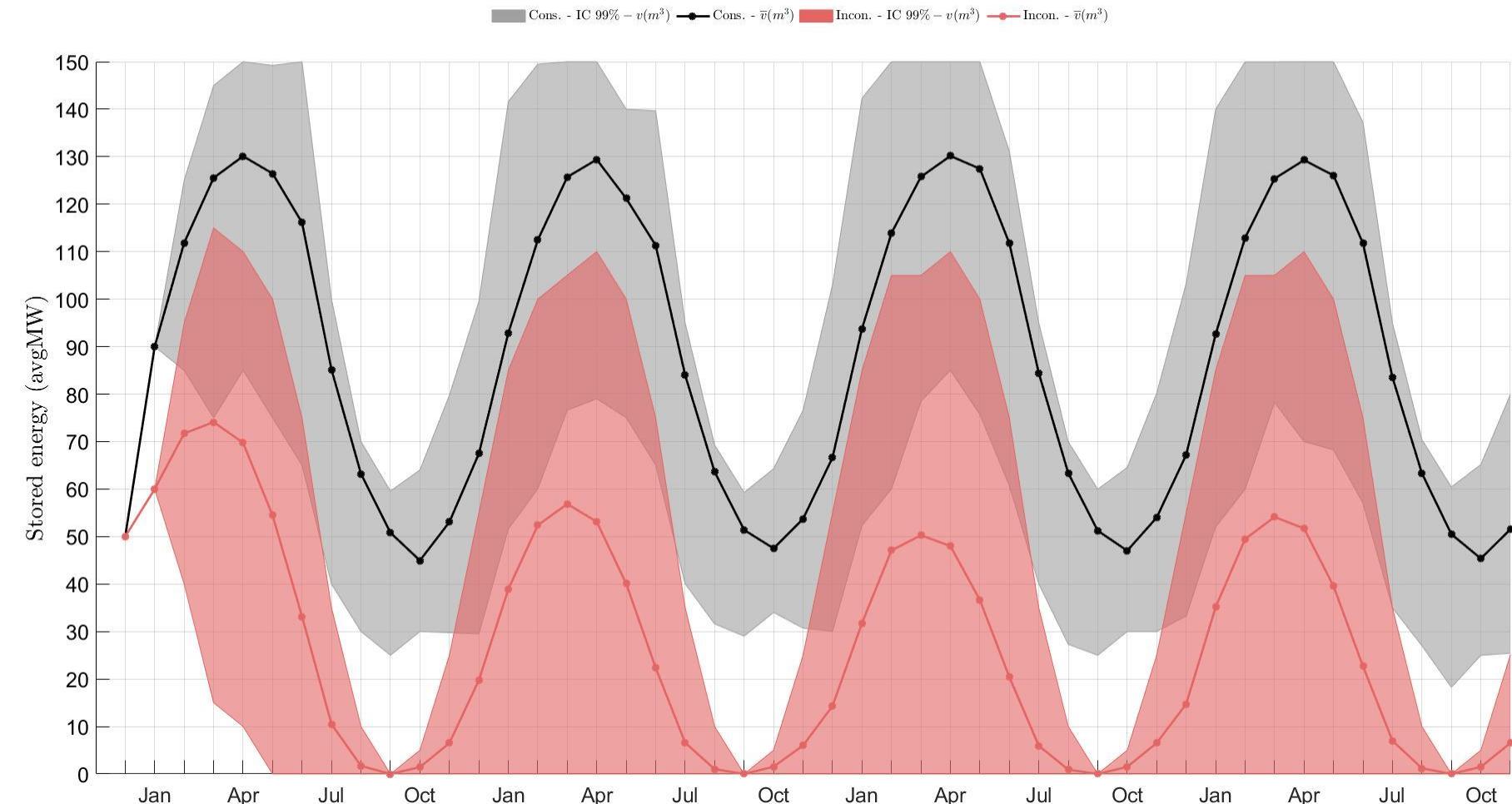
Thermal Generator	$c$ R\$/MWh	$\bar{G}$ MW
$G_1$	20	100
$G_2$	100	55
Hydro Generator	$\bar{V}$ $m^3$	$\bar{U}$ $m^3$
$H$	150	80

TL	From	To	$\bar{F}$ MW	Reactance (pu)
1	1	3	100	1
2	2	3	70	1
3	1	2	30	1

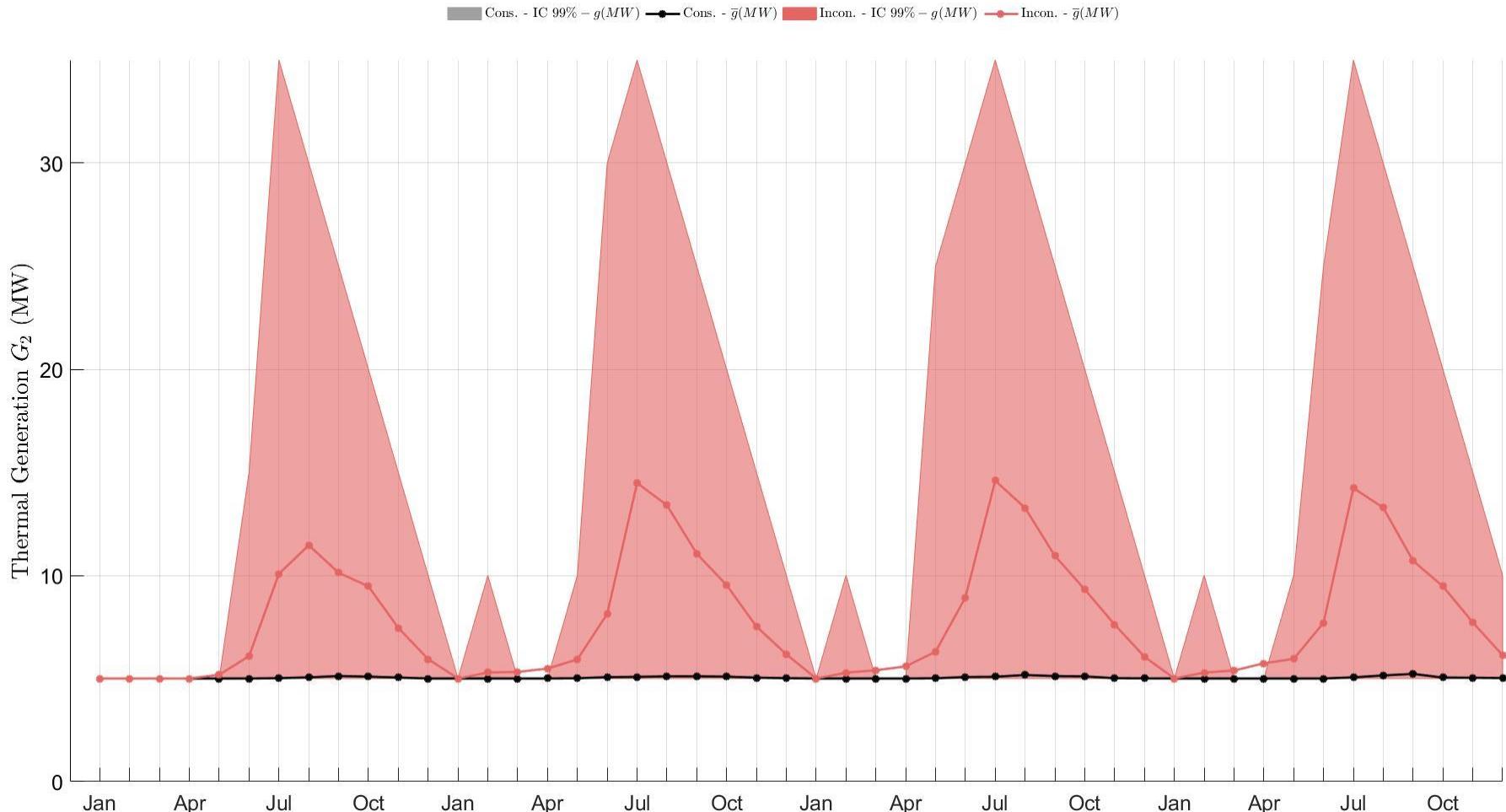
# GAP

**GAP: MMR\$1761.8**  
**GAP confidence interval: MMR\$[1737.9 1785.8]**

# Stored energy

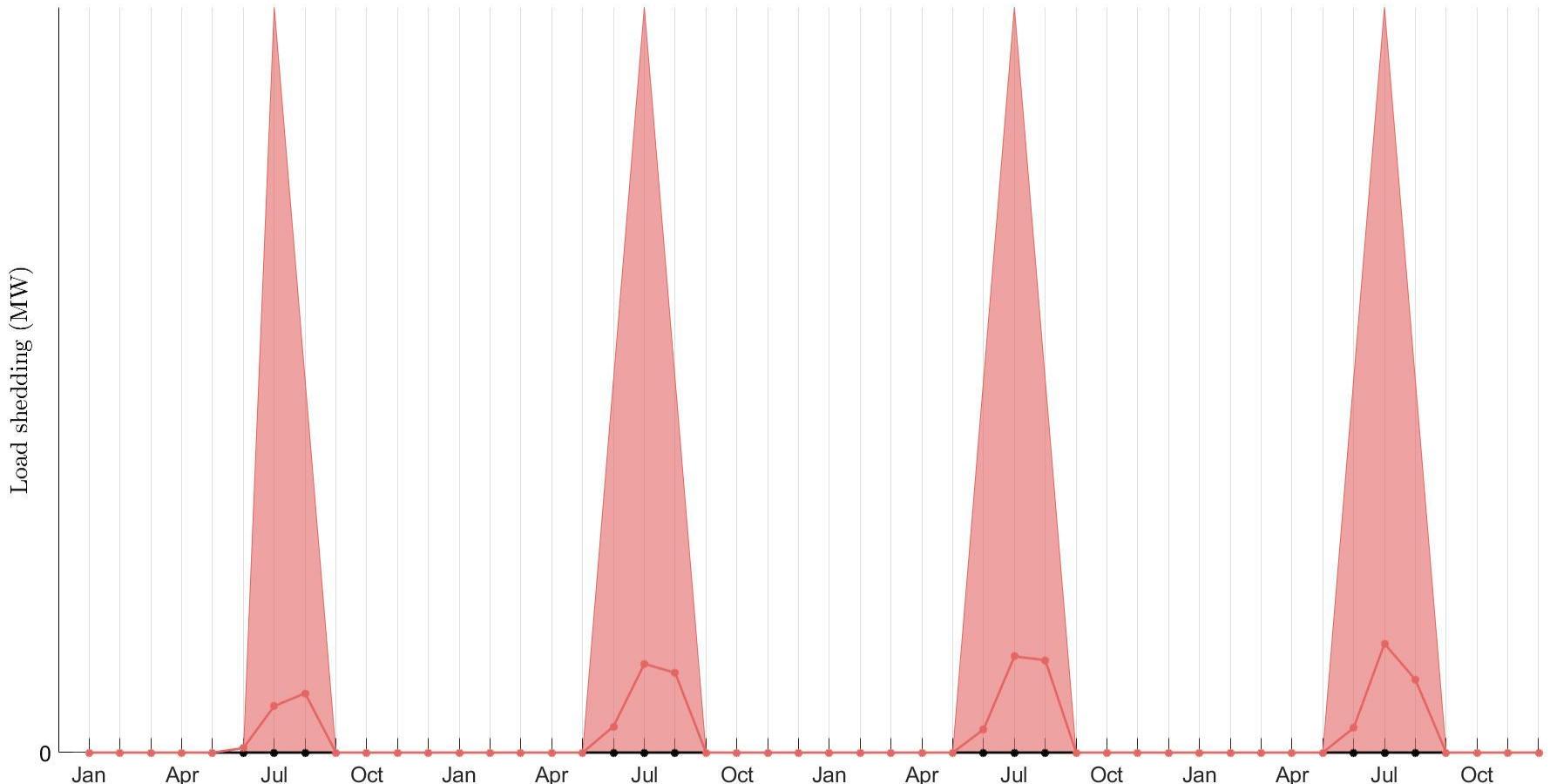


# Thermal Generation $G_2$



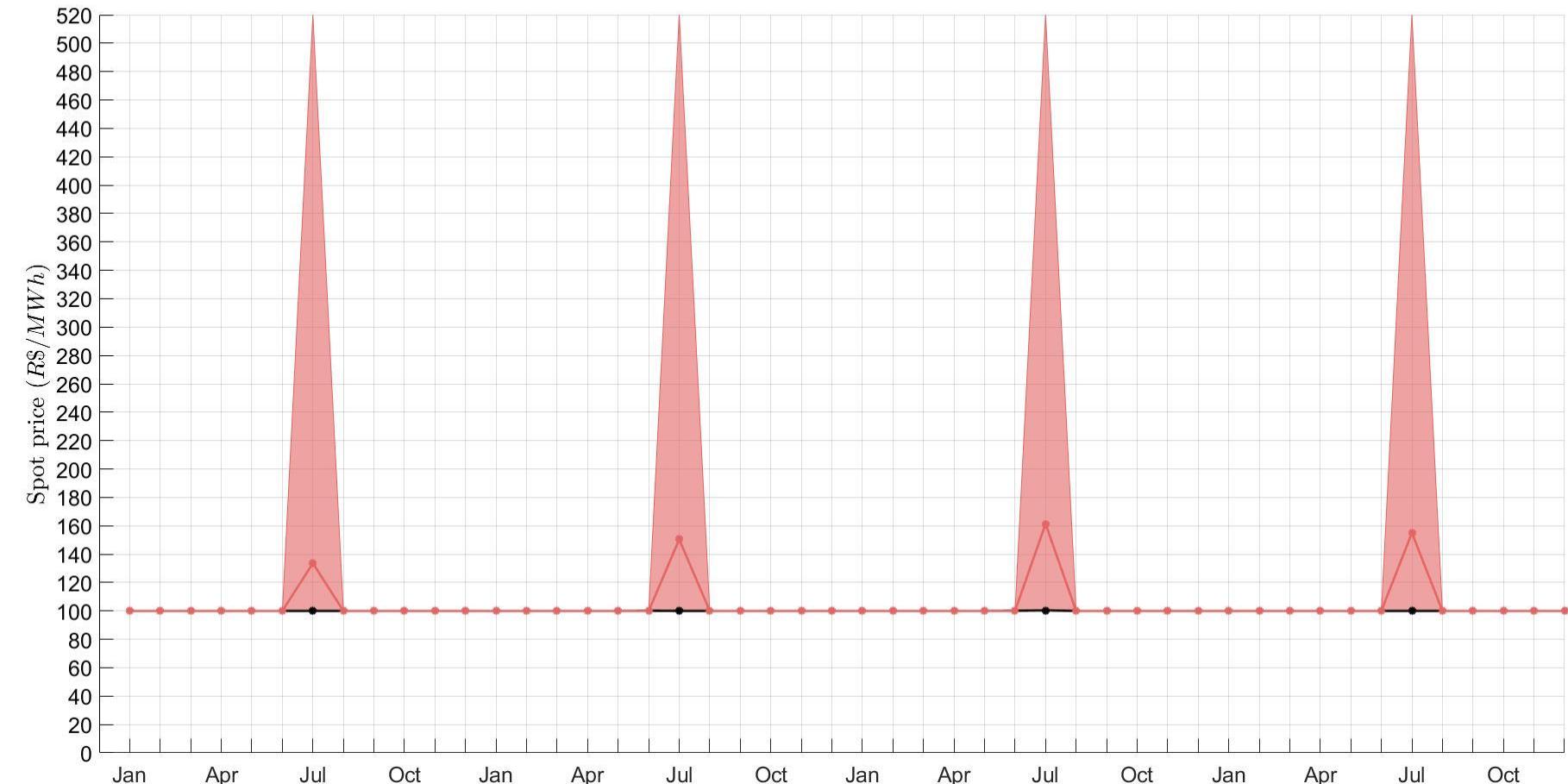
# Load shedding

■ Cons. - IC 99% -  $\delta(MW)$  ■ Cons. -  $\bar{\delta}(MW)$  ■ Incon. - IC 99% -  $\delta(MW)$  ■ Incon. -  $\bar{\delta}(MW)$

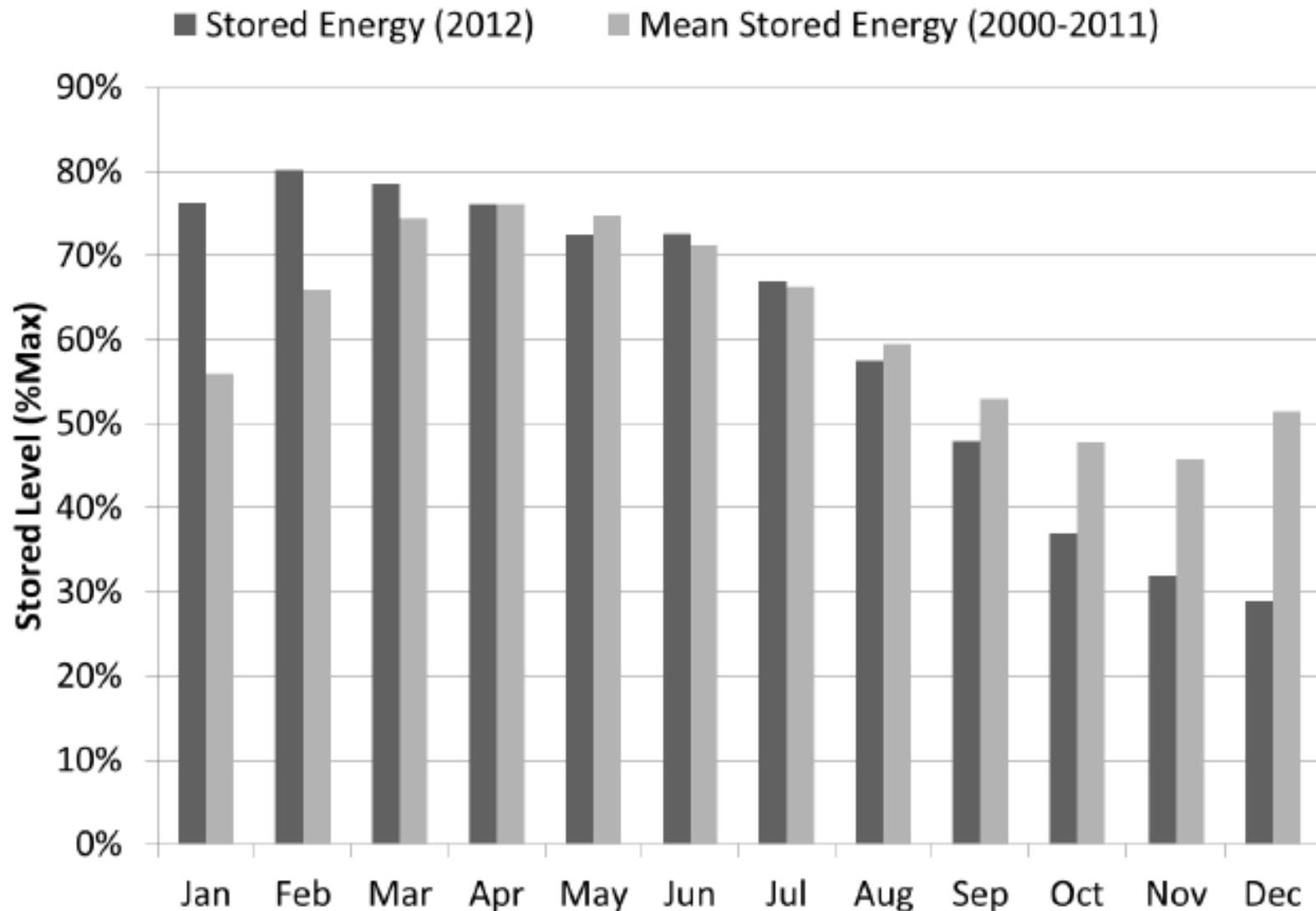


# Spot price

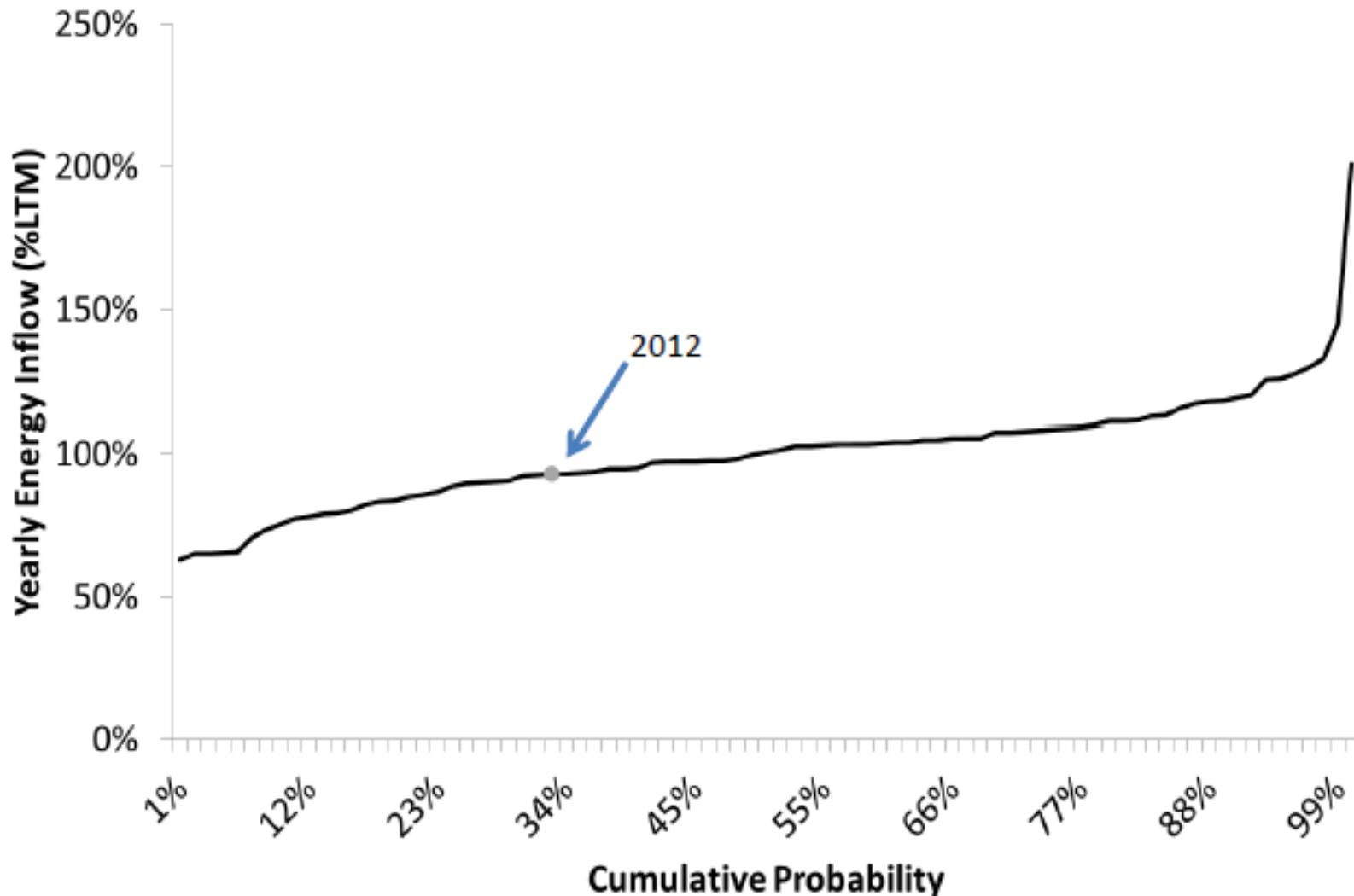
■ Cons. - IC 99% -  $\overline{\text{spot}}(R\$/MWh)$  ● Cons. -  $\overline{\text{spot}}(R\$/MWh)$  ■ Incon. - IC 99% -  $\overline{\text{spot}}(R\$/MWh)$  ● Incon. -  $\overline{\text{spot}}(R\$/MWh)$



# Stored Energy in the Brazilian Southeast Subsystem in 2012



# Inflow Energy in the SE Subsystem



# Inflow Energy in the SE Subsystem

